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(波浪部份)

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計畫主持人：所長 梁 乃 匡

研究人員：簡 仲 環

洪 憲 忠

蘇 青 和

吳 基

江 中 權

## 目 錄

一、引言 .....	1
二、季風有效影響區之設定 .....	2
三、由實測資料推求季風波浪經驗常數 .....	6
四、颱風湧浪週期推算法之探討 .....	12
五、等效風域法颱風波浪之推算 .....	23
六、結論與建議 .....	40
七、參考文獻 .....	41
八、附錄	
附錄 I 波浪預報程式	
附錄 II 可用於個人電腦之波浪預報系統程式	
附錄 III 颱風資料	
附錄 IV 蘇澳波浪資料	

## 一、引言

梁 乃 匡

本報告為四年波浪預報計畫的第三年成果。首先利用中央氣象局提供的冬季網格點風速風向資料，以及測站的波浪記錄，求出各站的經驗常數，然後用另一段資料來驗證。由於過去推算的湧浪週期並不理想，而週期影響湧浪到達的時間，因此加以重新探討；利用民國74~75年間8個颱風及在蘇澳測得的波浪資料，求出新的推算公式。本模式所採用的颱風波浪推算法為 Bretschneider 所提出，其中波浪場關係直接由所提出的圖迴歸而得。今仍依 Bretschneider 所提之基本公式，循等效風域觀念，重新計算波浪場關係，與舊的比較。

## 二、季風風場有效影響區之設定

簡 仲 璟

由於季風風場已網格式化，對於每一網格式可視為一波浪生成的單位元素風場。此網格式形狀近似正方形，隨緯度增大而有較大的變形，在本報告中是以梯形近似之，並假設在元素風場中的風速與風向均勻一致。對於元素風場所產生的波能，因為距離與時間差的關係，並不一定能全部到達吾欲推算波浪的位置，可能一部分或全部不到達，因此有所謂有效影響區之設定，如圖 2-1。設定方法說明如下：

情況(1)

$$\text{若 } |Ri-DD| \geq \frac{L}{2}(\sin\theta + \cos\theta)$$

$$\text{則 } Ai=0 \quad i=l, u$$

情況(2)

$$(a) \text{ 若 } |Ri-DD| \geq \frac{L}{2}(\cos\theta - \sin\theta)$$

$$\text{則 } Ai = \left( \frac{\frac{L}{2}(\sin\theta + \cos\theta) - |Ri-DD|}{L\sin\theta} \right)^2 \cdot \frac{L^2}{2} \tan\theta$$

$$(b) \text{ 若 } |Ri-DD| < \frac{L}{2}|\cos\theta - \sin\theta|$$

$$\text{則 } Ai = \left( \frac{L}{2}|\cos\theta - \sin\theta| - |Ri-DD| \right) \cdot \frac{L}{\cos\theta} + \frac{L^2}{2} \tan\theta$$

其中

下標  $i$  :  $l, u$

DD: 網格式中心點至推算點距離

L: 正方網格式邊長

Ri: 波能傳遞之下限距離

$R_u$ : 波能傳遞之上限距離

$A_l$ : 由  $R_l$  所求出之參考面積

$A_u$ : 由  $R_u$  所求出之參考面積

$\beta$ : 網格中心點至推算點之連線與 Y 軸之夾角

若  $\beta > 45^\circ$  則  $\theta = 90^\circ - \beta$

若  $\beta \leq 45^\circ$  則  $\theta = \beta$

若  $A_e$ : 表有效影響區之面積, 則

情況:

(1) 若  $R_l \leq DD$ , 且  $R_u \leq DD$

則  $A_e = A_u - A_l$

(2) 若  $R_l < DD$ , 且  $R_u > DD$

則  $A_e = L^2 - A_u - A_l$

(3) 若  $R_l > DD$  且  $R_u > DD$

則  $A_e = A_l - A_u$

因爲網格形狀隨緯度增加而變形, 而不是正方形, 因此  $A_e$  必須加以修正, 若  $A_c$  表真實網格面積, 則  $A_e$  修正如下:

$$A_{em} = A_e \cdot \frac{A_c}{L^2}$$

其中  $A_{em}$  表修正之有效影響區之面積。

茲舉一例說明, 例設風速 15 公尺/秒時間差 36 小時,  $D \cdot D = 2,000$  公里,

$\beta = 30^\circ$ , 風速資料時間隔 3 小時  $L = 111.12$  公里,  $A_c = 120,000$

則  $R_l = 15 \times 3600 \times 36 / 1000 = 1944$  公里

$R_u = 15 \times 3600 \times (36+3) / 1000 = 2106$  公里

$|R_l - DD| = 56$  公里

$|R_u - DD| = 106$  公里

$$\frac{L}{2} (\cos 30^\circ + \sin 30^\circ) = 75.9 \text{ 公里}$$

$$\frac{L}{2} |\cos 30^\circ - \sin 30^\circ| = 20.3 \text{ 公里}$$

$$\text{因 } |R_l - DD| = 56 < 75.9$$

$$|R_l - DD| = 56 > 20.3$$

$$\text{故 } A_l = \left( \frac{75.9 - 56}{111.12 \cdot \sin 30^\circ} \right)^2 \cdot \frac{111.12^2}{2} \tan 30^\circ = \left( \frac{19.9}{55.56} \right)^2 \cdot 3564.5 = 457.3 \text{ 平方公里}$$

$$|R_u - DD| = 106 > 75.9$$

$$\text{故 } A_u = 0$$

$$\text{因 } R_l = 1944 < 2000$$

$$R_u = 2106 > 2000$$

$$\text{則 } A_e = L^2 - A_u - A_l$$

$$= (111.12)^2 - 0 - 457.3$$

$$= 11890.4 \text{ 平方公里}$$

$$A_{em} = A_e \cdot \frac{A_c}{L^2} = 11890.4 \cdot \frac{120000}{12347.7} = 11555.6 \text{ 平方公里}$$

即有效影響區之面積為 11555.6 平方公里

有關有效影響區設立之程式見附錄一中之副程式 EAREA。

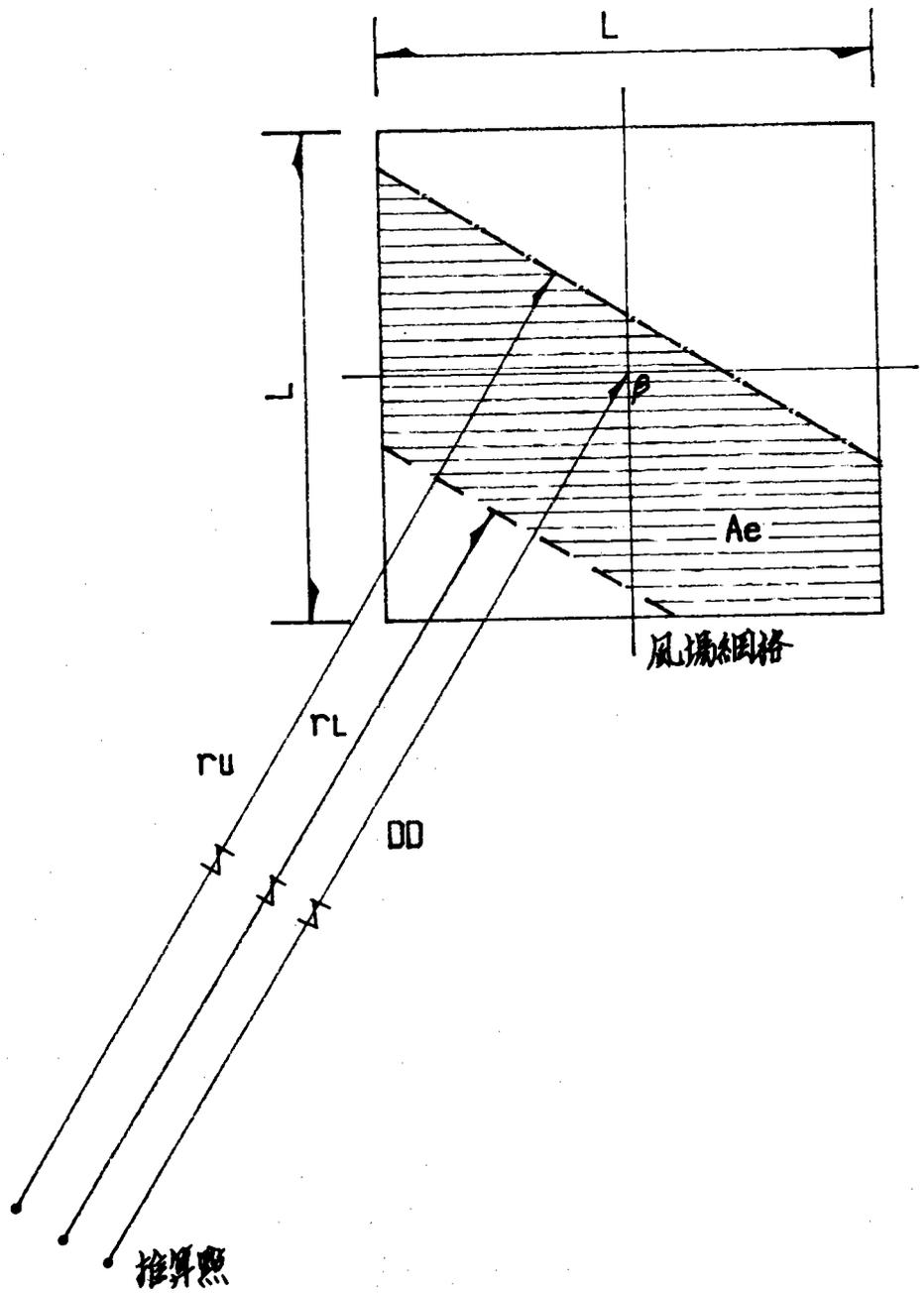


圖 2.1 風場有效影響區

### 三、由實測資料推求季風波浪經驗常數

簡仲環、洪憲忠、江中權

由於面積風域法主要觀點為考慮與浪之間的能量授受，因此我們藉著一段實測季風資料及對應的實測波浪資料，來決定能量授受關係，即經驗常數  $\bar{\xi}$ 。另外，決定推算週期公式：

$$\frac{gT_{1/3}}{2\pi\bar{U}} = C_2 \left( \frac{g \cdot \text{TDUR}}{\bar{U}} \right) C_1$$

$$\frac{gT_{1/3}}{2\pi\bar{U}} = C_4 \left( \frac{g \cdot F}{\bar{U}^2} \right) C_3$$

中的  $C_1$ ， $C_2$ ， $C_3$ ， $C_4$  值，其中  $\bar{U}$  為有效風域平均風速，TDUR 為吹風延時， $F$  為有效風域最長距離。通常經驗常數受各站地點，風域界定及季節的影響而稍有差異。推求經驗常數的風場資料為由 76/01/18~76/02/01 每三小時一筆，區域範圍則東經  $110^\circ$  至  $135^\circ$ ，北緯  $10^\circ$ ~ $40^\circ$ ，相對應的波浪資料為由 76/01/23~76/02/01 共有鼻頭角、新港、東吉島、小琉球四個波浪站。由此所求得之經驗常數值如表 3.5。

以面積風域法推算季風波浪之前，此經驗常數必須先求得，然後再以此常數反推算出季風波浪。推算結果與實測比較如表 3.1，3.2，3.3，3.4。由表中可發現推算結果頗合理，但由於所取風場資料為三小時一筆故推算實測值變動較小。以後或許可變風資料之時間間距。由四個站的推算結果發現鼻頭角波浪最大，新港、東吉島次之，小琉球最小，此與實測結果有相同的趨勢，以後應繼續此工作而得更佳之經驗常數值並對其他波浪測站，也進行常數值的求得，及颱風發生時，季風波浪與颱風波浪的合成進行驗證，及調整。

波浪預報程式有二，適用於 VAX—11 780 者，如附錄 I，適用於 IBM 個人電腦者，如附錄 II 所示。

表 3.1 測站：鼻頭角

時 間	量 測 值		推 算 值	
	波高( $H_{1/3}$ )公尺	週期( $T_{1/3}$ )秒	波高( $H_{1/3}$ )公尺	週期( $T_{1/3}$ )秒
76/02/23:14	1.09	6.0	1.5	6.7
76/02/23:17	0.85	6.0	1.4	6.7
76/02/23:20	0.84	6.2	1.3	6.7
76/02/23:23	0.87	5.9	1.3	6.7
76/02/24:02	0.93	5.5	1.2	6.7
76/02/24:05	1.25	5.5	1.7	6.7
76/02/24:08	1.00	5.7	1.7	6.7
76/02/24:11	1.12	5.8	1.5	6.7
76/02/24:14	1.09	5.7	1.3	6.7
76/02/24:17	1.11	6.1	1.1	6.7
76/02/24:20	1.25	6.3	1.0	6.7
76/02/24:23	1.78	6.3	1.1	

表 3.2 測站：新港

時 間	量 測 值		推 算 值	
	波高( $H^{1/3}$ )公尺	週期( $T^{1/3}$ )秒	波高( $H^{1/3}$ )公尺	週期( $T^{1/3}$ )秒
76/02/23:14	1.24	6.7	1.5	8.1
76/02/23:17	1.08	6.8	1.5	8.0
76/02/23:20	1.00	7.0	1.4	7.8
76/02/23:23	1.01	7.2	1.6	7.7
76/02/24:02	0.81	7.3	1.5	7.9
76/02/24:05	0.84	7.5	1.6	7.9
76/02/24:08	0.88	7.6	1.4	7.8
76/02/24:11	1.04	6.6	1.5	7.6
76/02/24:14	1.30	6.9	1.5	7.6
76/02/24:17	1.24	6.6	1.2	7.8
76/02/24:20	1.37	7.1	1.3	7.7
76/02/24:23	1.45	7.1	1.4	7.7

表 3.3 測站：東吉島

時 間	量 測 值		推 算 值	
	波高( $H_{1/3}$ )公尺	週期( $T_{1/3}$ )秒	波高( $H_{1/3}$ )公尺	週期( $T_{1/3}$ )秒
76/02/23:14	1.21	5.6	0.91	8.1
76/02/23:17	1.12	5.7	0.62	8.9
76/02/23:20	0.86	5.5	0.68	8.0
76/02/23:23	1.08	5.3	0.83	7.6
76/02/24:02	0.74	4.8	0.81	6.8
76/02/24:05	0.62	5.5	0.90	6.1
76/02/24:08	0.40	4.4	0.85	6.9
76/02/24:11	0.66	4.3	0.78	7.3
76/02/24:14	0.73	4.4	0.89	6.9
76/02/24:17	0.93	4.8	0.94	6.4
76/02/24:20	0.80	4.7	1.16	5.5
76/02/24:23	1.22	4.9	1.10	5.7

表 3.4 測站：小琉球

時 間	量 測 值		推 算 值	
	波高( $H_{1/3}$ )公尺	週期( $T_{1/3}$ )秒	波高( $H_{1/3}$ )公尺	週期( $T_{1/3}$ )秒
76/02/23:14	0.68	4.8	0.55	6.1
76/02/23:17	0.83	4.5	0.44	5.9
76/02/23:20	0.80	4.5	0.5	6.0
76/02/23:23	0.57	4.8	0.5	5.8
76/02/24:02	0.64	4.4	0.5	5.8
76/02/24:05	0.70	4.0	0.6	5.7
76/02/24:08	0.61	4.3	0.6	5.6
76/02/24:11	0.58	3.8	0.6	5.6
76/02/24:14	0.85	3.7	0.6	5.6
76/02/24:17	1.03	4.2	0.6	5.6
76/02/24:20	0.72	4.5	0.7	5.6
76/02/24:23	0.51	4.4	0.6	5.6

表 3.5 各測站之經驗常數

測站	常數	$\xi$ 值	$C_1$	$C_2$	$C_3$	$C_4$
鼻頭角		0.29E - 04	0.42E + 00	0.29E - 05	0.13E + 00	0.21E - 05
新港		0.26E - 04	0.26E + 00	0.59E - 05	-0.59E - 01	0.31E - 05
東吉島		0.24E - 04	- 0.12E - 00	0.74E - 05	-0.54E + 00	0.45E - 05
小琉球		0.96E - 05	0.13E + 00	0.53E - 05	-0.18E + 00	0.28E - 05

#### 四、颱風湧浪週期推算法之探討

梁 乃 匡

##### 4-1 引言

梁乃匡 (1982) 曾提出一個颱風湧浪預報法，其主要觀念是把颱風波浪場當作點波源來看，颱風中心波浪由 Bretschneider 方法估計 (1976)。推算公式如下：

$$H^{1/3} = C \quad H_R^* \sqrt{\frac{R}{DD}} \quad (4-1)$$

其中

$H^{1/3}$  颱風湧浪代表波波高，單位米

$C$  經驗常數，約 0.11

$H_R^*$  移動颱風在最大風速半徑  $R$  處風向指向測站處的代表波高，單位呎

$R$  最大風速半徑，單位哩

$DD$  颱風中心到測站的距離，單位哩

$$T^{1/3} = C' T_{RS} \quad (4-2)$$

其中

$T^{1/3}$  颱風湧浪代表波週期，單位秒

$T_{RS}$  在 Bretschneider 方法中與  $H_R^*$  有關的颱風波浪週期，單位秒

$C'$  經驗常數，由下式求得：

$$C' = 0.05 \frac{DD \cdot T_{RS}}{R \cdot U_{RS}^*} + 1 \quad (4-3)$$

其中

$U_{RS}^*$  為移動颱風的海面上 10 米高 10 分鐘平均風速，單位節

(4-3) 式後來被梁乃匡及簡仲環 (1984) 由相同資料修改為下式：

$$C' = 0.0021 \left( \frac{DD \cdot T_{RS}}{R \cdot U_{RS}^*} \right)^2 + 0.0012 \left( \frac{DD \cdot T_{RS}}{R \cdot U_{RS}^*} \right) + 1.21 \quad (4-4)$$

彭海鯤 (1985) 建議用  $\frac{(DD \cdot T_{RS})^{1/2}}{(R \cdot U_{RS}^*)^2}$  代替  $\frac{DD \cdot T_{RS}}{R \cdot U_{RS}^*}$  作為參數來求  $C'$ ，

然而前者非為無因次，在因次分析上無意義。

由於湧浪週期影響湧浪抵達的時間及由於堆積與消退所造成的波高修正係數  $\lambda$ ，而過去湧浪週期推算結果不盡理想，有進一步探討的必要。

#### 4-2 新的無因次參數

如上所述，目前  $T^{1/3}/T_{RS}(=C')$  與  $\frac{DD \cdot T_{RS}}{R \cdot U_{RS}^*}$  被用來作為預測湧浪週期的無因次參數，表面上看  $T_{RS}/U_{RS}^*$  為非無因次，但因波相速度  $C$  與週期  $T_{RS}$  成正比，所以  $T_{RS}/U_{RS}^*$  也是無因次的，然而， $T^{1/3}/T_{RS}$  與  $\frac{DD \cdot T_{RS}}{R \cdot U_{RS}^*}$  均有  $T_{RS}$ ，這並非一個好的安排。因為最大風速半徑  $R$  在計算  $T_{RS}$  與  $U_{RS}^*$  時已經用上，所以  $R$  可以去掉，如此剩下  $T^{1/3}$ ， $T_{RS}$ ， $DD$  與  $U_{RS}^*$  四個物理量，很容易就配出兩組新的無因次參數來： $T^{1/3}/U_{RS}^*$  與  $DD/T_{RS}^2$  及  $T^{1/3}/T_{RS}$  與  $DD/U_{RS}^{*2}$  前者的物理意義是湧浪波速與颱風中心最大風速的比值，及代表颱風中心與測站間波長的倍數。後者表示湧浪週期與風浪週期之比及代表測站與颱風中心距離的無因次長度（分子應乘重力加速度  $g$ ，因係常數故省略）。

因為在觀念上假設颱風波浪場為一點波源，所以由颱風移動而造成在颱風波浪場的變化也許不重要，因此未考慮颱風移動的  $T_R$  與  $U_{RS}$  可以取代  $T_{RS}$  與  $U_{RS}^*$ ，如此則有  $(T^{1/3}/T_R, \frac{DD \cdot T_R}{R \cdot U_{RS}^*})$ ， $(T^{1/3}/T_R, \frac{DD \cdot T_R}{R \cdot U_{RS}})$ ， $(T^{1/3}/T_R, \frac{(DD \cdot T_R)^{1/2}}{(R \cdot U_{RS}^*)^2})$ ， $(T^{1/3}/U_{RS}^*, \frac{DD}{T_R^2})$ ， $(\frac{T^{1/3}}{T_R}, \frac{DD}{U_{RS}^2})$ ， $(\frac{T^{1/3}}{U_{RS}}, \frac{DD}{T_R^2})$  六組參數對可供選擇，很幸運的，1985—1986 兩年間在蘇澳測得 8 個颱風的湧浪，這 8 個颱風的資料如附錄 III 的表中，相關的波浪資料在附錄 IV 的表中。

上述六組參數將利用實測資料作其相關性分析，相關性最大的就是最好的參數。今有  $A$ 、 $B$  兩隨機變數，其相關係數 (Correlation Coefficient) 的定義如下：

$$\text{Correlation Coefficient} = \frac{\text{Cov}\{A, B\}}{\sigma_A \cdot \sigma_B} \quad (4-5)$$

其中  $\sigma_A$  與  $\sigma_B$  為  $A$  與  $B$  的標準偏差，相關係數的絕對值永遠小於 1，對  $N$  個有限資料而言，

$$\begin{aligned} \text{Correlation Coef} &= \frac{\sum_1^N (A-\bar{A})(B-\bar{B}) / (N-1)}{\left(\frac{1}{N-1}\right)^{1/2} \left(\frac{1}{N-1}\right)^{1/2}} \\ &= \frac{\sum_1^N (A-\bar{A})(B-\bar{B})}{\left(\sum_1^N (A-\bar{A})^2\right)^{1/2} \left(\sum_1^N (B-\bar{B})^2\right)^{1/2}} \quad (4-6) \end{aligned}$$

其中  $\bar{A}$  與  $\bar{B}$  爲 A 與 B 的平均值。

找尋颱風與其相關的波浪資料的方法，如同以往一樣由  $T_{1/3}$  的群波速度，即 1.56  $T_{1/3}$  節來追遡颱風中心的位置，如非恰好相等，則以內插法求出  $T_{1/3}$ 。由於吾人相信湧浪週期  $T_{1/3}$  必然大於颱風中心風浪週期  $T_R$  或  $T_{RS}$ ，因此當得到的  $T_{1/3}$  小於  $T_R$  或  $T_{RS}$  則捨去，因為湧浪很可能被當地短週期風浪所“污染”而變小。另外，當距離誤差在 50 哩以上者亦捨去。由 8 個颱風一共採集了 69 個樣品，求得的相關係數如表 4-1 所示，以  $(T_{1/3}/U_{RS}, DD/T_R^2)$  的相關最好。

表 4-1 各參數間相關係數

參數	相關係數
$\frac{T_{1/3}}{T_R} \& \frac{DD \cdot T_R}{R \cdot U_{RS}^*}$	0.305
$\frac{T_{1/3}}{T_R} \& \frac{DD \cdot T_R}{R \cdot U_{RS}}$	0.316
$\frac{T_{1/3}}{T_R} \& \frac{(DD \cdot T_R)^{1/2}}{(R \cdot U_{RS})^2}$	0.55
$\frac{T_{1/3}}{U_{RS}^*} \& \frac{DD}{T_R^2}$	0.485
$\frac{T_{1/3}}{T_R} \& \frac{DD}{U_{RS}^2}$	0.514
$\frac{T_{1/3}}{U_{RS}} \& \frac{DD}{T_R^2}$	0.626

用  $U_{RS}$  比  $U_{RS}^*$  要好， $\frac{T_{1/3}}{T_R} \& \frac{(DD \cdot T_R)^{1/2}}{(R \cdot U_{RS})^2}$  爲次優。

#### 4-3 新的湧浪推算公式

由上節知參數對  $\frac{T^{1/3}}{U_{RS}}$  &  $\frac{DD}{T_R^2}$  的相關最高將 69 組資料列在表 4-2，並點繪在圖 4-1，資料點仍然很散，其原因很可能是部份湧浪被當地短週期波浪所“污染”而變小所致，因此最好由波譜求出湧浪週期來取代波週期  $T^{1/3}$ 。在圖 4-1 上的資料點中取兩條曲線。其一取包絡線，假設較大值的資料未被當地風浪所“污染”，代表真正的湧浪週期，其二取中間值，假設無上述情況。

因  $\frac{DD}{T_R^2}$  大於 20 者很少，因此假設  $\frac{DD}{T_R^2} > 20$  時  $\frac{T^{1/3}}{U_{RS}}$  取常數。迴歸出二方程式如下：

表 4-2 無因次參數原始資料

颱風名	年	月	日	時	$T^{1/3} / U_{RS}$	$DD / T_R^2$	註	
HAL	1985	6	20	8	0.32	12.1		
				14	0.29	9.8		
				20	0.28	8.5		
				21	2	0.29	7.7	
				8	0.26	6.2		
				14	0.24	5.4		
				20	0.23	4.2		
IRMA	1985	6	27	14	0.33	11.4		
				20	0.27	9.1		
				28	2	0.21	7.5	
NELSON	1985	8	18	20	0.33	16.5		
				19	2	0.27	12.9	
				8	0.27	11.8		
				14	0.28	11.2		
				20	0.25	9.4		
				20	2	0.25	8.7	
			8	0.26	8.1			

				14	0.23	7.0
			21	2	0.23	5.9
				8	0.23	5.3
				14	0.22	4.2
				20	0.22	3.6
			22	2	0.21	2.7
				8	0.22	2.2
				14	0.23	1.6
				20	0.22	1.1
VERA	1986	8	15	8	0.52	15.9
				14	0.39	12.8
				20	0.41	12.5
			16	2	0.45	11.9
				14	0.36	11.7
				20	0.33	10.3
			17	2	0.30	10.2
				14	0.38	13.0
			18	2	0.37	15.8
				8	0.28	11.8
			23	8	0.16	9.2
				14	0.17	9.1
				20	0.18	8.5
			24	2	0.18	8.1
ABBY	1986	9	14	20	0.42	20.4
			15	2	0.44	19.2
				8	0.35	13.9
				14	0.35	12.5
			17	20	0.20	2.8
			18	2	0.20	2.4
				8	0.21	2.1

表 4-2 (續)

颱風名	年	月	日	時	$T_{\frac{1}{3}} / U_{RS}$	$DD / T_R^2$	註		
BRENDA	1985	10	1	20	0.26	9.8			
				2	8	0.28	8.1		
					14	0.29	7.3		
					20	0.33	6.6		
				3	2	0.35	5.7		
					8	0.29	3.7		
					14	0.27	2.7		
					20	0.27	1.9	颱風接近	
				4	2	0.29	1.2	"	
					8	0.23	0.6	"	
					14	0.22	1.0	"	
				DOT	1985	10	14	8	0.43
14	0.38	26.7							
20	0.27	18.8							
15	2	0.27	17.8						
	8	0.20	13.0						
SARAH	1986	7	31					20	0.44
				8	1	2	0.31	10.1	
					8	0.42	12.1		
					14	0.39	10.6		
					20	0.39	10.0		
				2	2	0.39	9.9		

### 包絡線

$$\frac{T_{1/3}}{U_{RS}} = 0.2 + 0.023 \frac{DD}{T_R^2} - 0.0005 \frac{(DD)^2}{T_R^4}, \quad \frac{DD}{T_R^2} \leq 20 \quad (4-7)$$

$$\frac{T_{1/3}}{U_{RS}} = 0.46 \quad \frac{DD}{T_R^2} > 20$$

### 中間值曲線

$$\frac{T_{1/3}}{U_{RS}} = 0.18 + 0.0155 \frac{DD}{T_R^2} - 0.00025 \frac{(DD)^2}{T_R^4}, \quad \frac{DD}{T_R^2} \leq 20 \quad (4-8)$$

$$\frac{T_{1/3}}{U_{RS}} = 0.39 \quad \frac{DD}{T_R^2} > 20$$

### 4-4 驗證

採取 1980 年五個颱風 — IDA, KIM, NORRIS, PERCY 及 BETTY, 用式 (4-7) 及 (4-8) 推算湧浪週期, 再與在南灣用壓力式波高計所測週期比較, 點繪於圖 4-2, 4-3 上, (其中當  $T_{1/3}$  小於  $T_R$  即令  $T_{1/3} = T_R$ ), 由圖看出除了另有原因外, 由包絡線方程式 (式 (4-7)) 所算出的值與實測值比較吻合。

### 4-5 結論

(1)  $\frac{T_{1/3}}{U_{RS}}$  與  $\frac{DD}{T_R^2}$  為最佳的無因次參數, 由 8 個颱風, 69 組資料, 取包

絡線迴歸求得經驗式如下:

$$\frac{T_{1/3}}{U_{RS}} = 0.2 + 0.023 \frac{DD}{T_R^2} - 0.0005 \frac{(DD)^2}{T_R^4}, \quad \frac{DD}{T_R^2} \leq 20$$

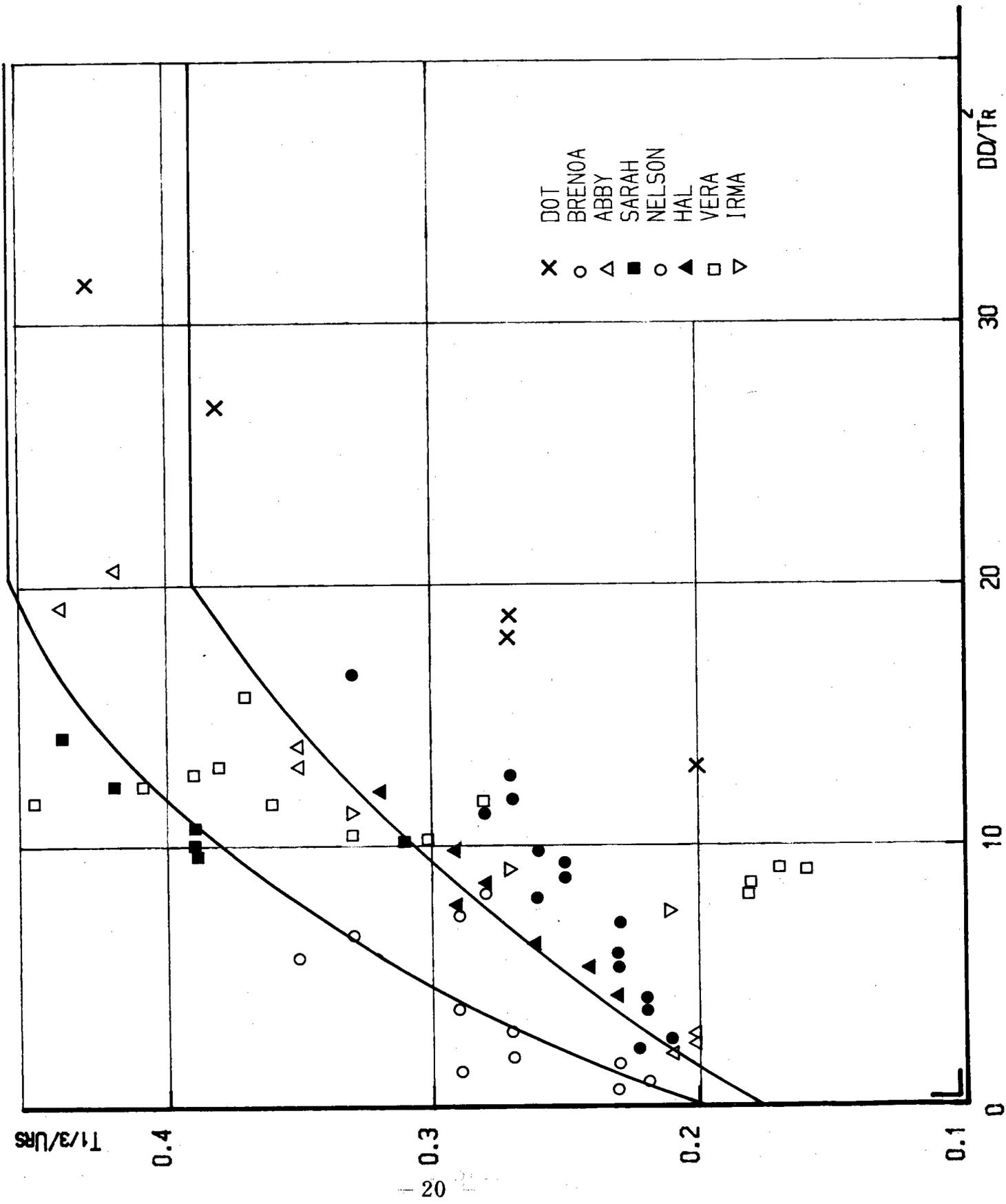
$$\frac{T^{1/3}}{U_{RS}} = 0.46$$

$$\frac{DD}{T_R^2} > 20$$

經與實測資料比較，頗為吻合。

(2)一般實測波浪資料湧浪與當地風浪混在一起，因此實際湧浪週期應大於  $T^{1/3}$ 。所以，以後應計算波譜，求出湧浪週期代替  $T^{1/3}$ 。

(3)當颱風太近時，本方法已不能應用。



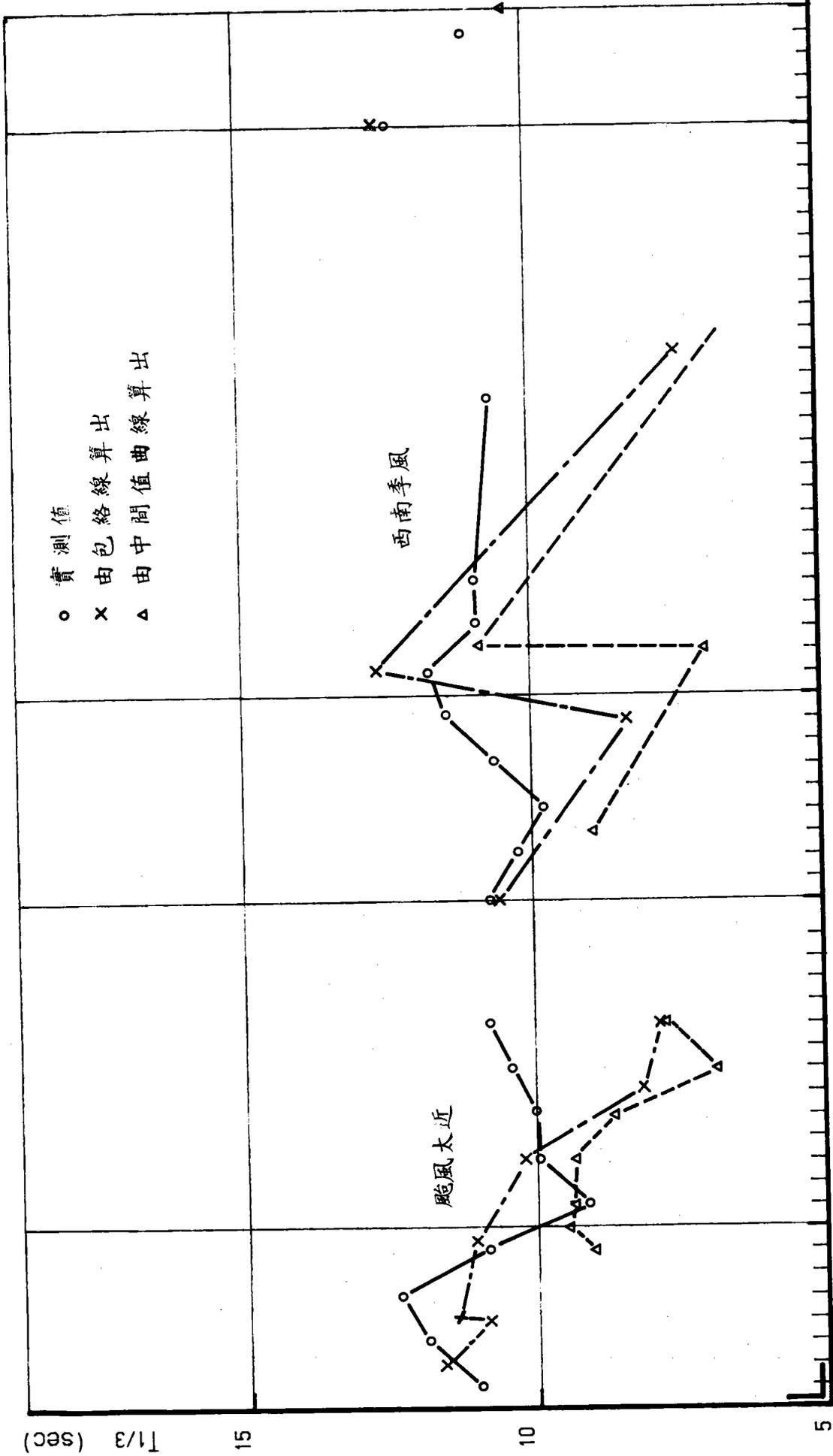
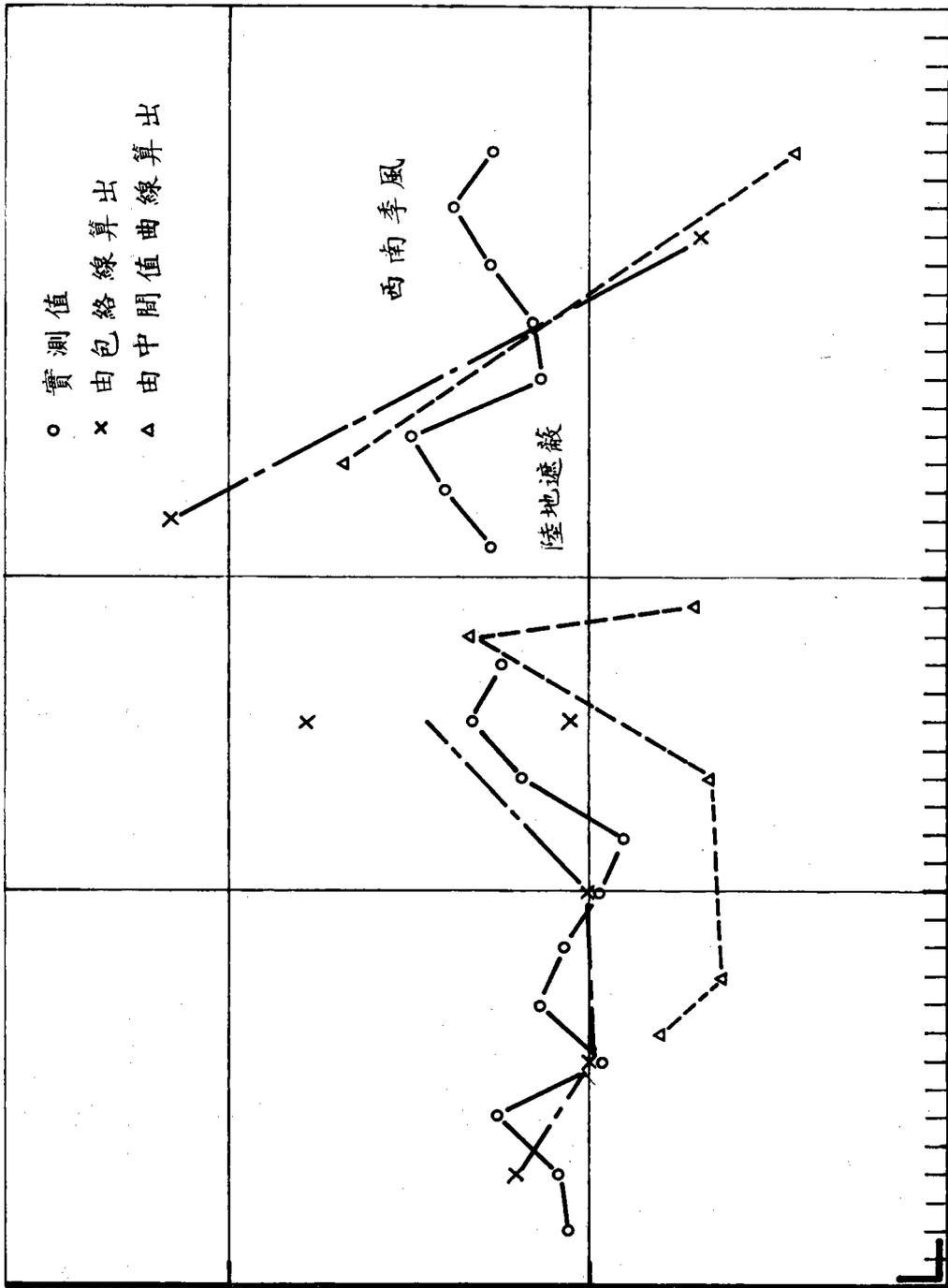


圖 4-2 湧浪週期推算與實測比較

T<sub>1/3</sub> (sec)



9月17日  
1980年

PERCY

11月6日  
1980年

BETTY

圖 4-3 湧浪週期推算與實測比較 (續)

## 五、等效風域法颱風波浪之推算

吳 基

### 1. 引言

所謂等效風域法在基本上是應用 Bretschneider 在 1979 年發表的 " The Two - Direction Significant Wave Forecasting Model With Special Application to U.S. Weather Service Hurricane Wind Model " 中各個基本公式, 而以等效風域之觀念推算颱風風場內波浪場之狀況, 有關各個基本公式及相關圖表、常數, 請直接參閱該文, 在此不多贅述。

## 2. 等效風域 (Equivalent Fetch) 法之原理

由於穩定颱風係屬一種滯留，穩定狀態之風場，故其波浪場分佈的情形僅為半徑  $r$  之函數，由最大風速半徑處往外，波高逐漸遞減（註：依照 Bretschneider 之推算，在  $2R$  處，可能有較大之代表波高出現），故我們可以由最大風速半徑  $R$  處往外，延半徑方向繪一直綫至外圍圓周，如能計算出此綫上各點之代表波高分佈，則穩定颱風風場內任一點之波浪分佈均能推得。

現說明等效風域法之原理如下：

假設一條直綫上各點之風速、風向、兩點間之距離均為已知，如圖 5-1 所示，則 B 點之代表波高  $H_B$  可由 A 點之風速延此綫之分量與吹風距離（此時為  $\Delta x$ ）所決定，即

$$\frac{gH_B}{U_A U_A \cos(\alpha_A)} = 0.283 \tanh \left[ 0.0125 \left( \frac{g\Delta x}{U_A U_A \cos(\alpha_A)} \right)^{0.42} \right]$$

得出  $H_B$  之後，再利用同樣的式子，以  $U_B$  取代  $U_A$ ， $\alpha_B$  取代  $\alpha_A$ ， $\Delta x$  則以  $F_{AB}$  代替，則可反求出  $F_{AB}$

$$F_{AB} = \frac{U_B U_B \cos(\alpha_B)}{g} \cdot \left[ \frac{1}{0.0125} \tanh^{-1} \left( \frac{gH_B}{0.283 U_B U_B \cos(\alpha_B)} \right) \right]^{\frac{1}{0.42}}$$

此處之  $F_{AB}$  即代表在同樣波高之前題下，以 B 點之風取代 A 點之風所得之等效風域 (Equivalent Fetch)。

接下來欲求 C 點之代表波高  $H_C$  則可用 B 點之風  $U_B$  及有效風域（此時為  $\Delta x + F_{AB}$ ）代入基本公式(1)而得，而  $H_C$  又可以 C 點之風  $U_C$  代回原式得出等效風域  $F_{AC}$ ，依次類推則 B、C、D、E、F 各點之代表波高均可推得

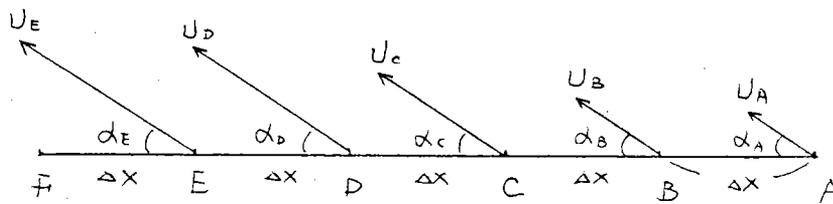


圖 5-1 等效風域之推算原理

### 3. 推算之步驟

依據 Bretschneider 之經驗公式，在 XY 座標平面上任一點之波高均可由 X 方向上來的分量  $H_x$  及 Y 方向上來的分量  $H_y$  以能量疊加之方式合成，即  $HH = (H_x^2 + H_y^2)^{1/2}$ ，故實際推算步驟如下：

- ①繪出代表穩定颱風之圓形風場，以圓心為原點 0，決定 X、Y 軸得到四個象限，預定用於推算之象限為第四象限。
- ②延 +X 軸及 -Y 軸，自 1R 開始至 NR 為止，以  $R/5$  為間隔等分成 5N 段，(N 可自行設定，若定為 14，表示風場邊緣定於 14R 處根據實際推算之結果顯示，N 之值定為 10 至 14 較為適宜參見圖 5-2)，並繪成網格點，圖 5-3 是一個簡化了的圖形，僅分割成 5 段，實際推算時 X、Y 軸上各有 50~70 段。
- ③將模式颱風或實測颱風之重要氣象參數輸入，並利用基本公式推算 X 軸上各點之風速  $U(IC, 1)$ 。(IC = 5N, 5N-1, …… 5 IC = 5 時，即為最大風速半徑處)。
- ④由 X 軸上最外點向內，依等效風域之觀念依序推算各點之  $H_x$  ( $H_{1/3}$  之 X 軸方向上分量)即  $H_x(IC-1, 1) \Rightarrow H_x(IC-2, 1) \Rightarrow \dots \Rightarrow H_x(5, 1)$ 。
- ⑤利用三角函數關係計算正交於 X 軸上各點之 Y 軸平行綫上各網格點之位置角 ( $\theta$ )，距圓心距離，風向與 Y 軸平行綫之夾角，並推算出各點之風速。
- ⑥依等效之風域之觀念，由 Y 軸平行綫上圓周之點向上逐步推算出各點之  $H_y$  ( $H_{1/3}$  在 Y 軸平行綫上之分量)直到抵達 X 軸為止。

$$H_y(IC, ID) \Rightarrow H_y(IC, ID-1) \Rightarrow \dots \Rightarrow H_y(IC, 1)$$

- ⑦將 X 軸上各點所得之  $H_x(IC, 1)$  與  $H_y(IC, 1)$  合成，即

$$HH(IC, 1) = \sqrt{H_x(IC, 1)^2 + H_y(IC, 1)^2} \quad IC = 5N-1, 5N-2, \dots, 5$$

- ⑧以此推算所得之穩定颱風風場為基本架構，考慮颱風移動方向及速度，則可推算出移動風場內任一點之代表波波高狀態。

一般而言，移動颱風與穩定颱風比較，其右半圓，波高會變大，而左側則會減小。

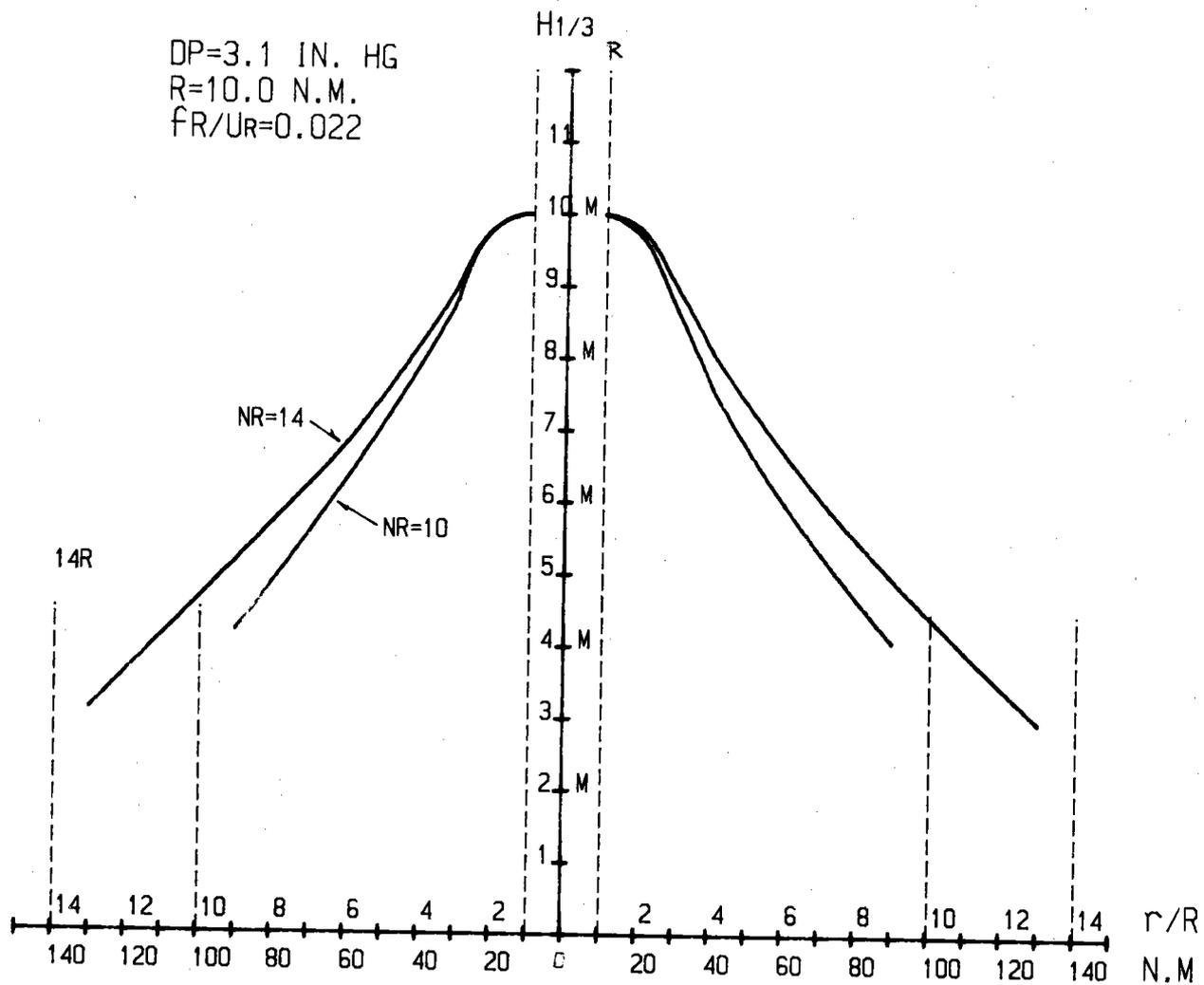


圖 5 - 2 以不同 NR 值推算穩定颱風風場內波高分佈

圖 5-3 STATIONARY HURRICANE

波浪場之推算

$$\frac{gH_x}{UU_x} = A_1 \tanh[B_1 \left( \frac{gF_x}{UU_x} \right)^{m_1}]$$

$$F_x = \frac{UU_x}{g} \left( \frac{1}{B_1} \tanh^{-1} \left( \frac{1}{A_1} \left( \frac{gH_x}{UU_x} \right) \right) \right)^{\frac{1}{m_1}}$$

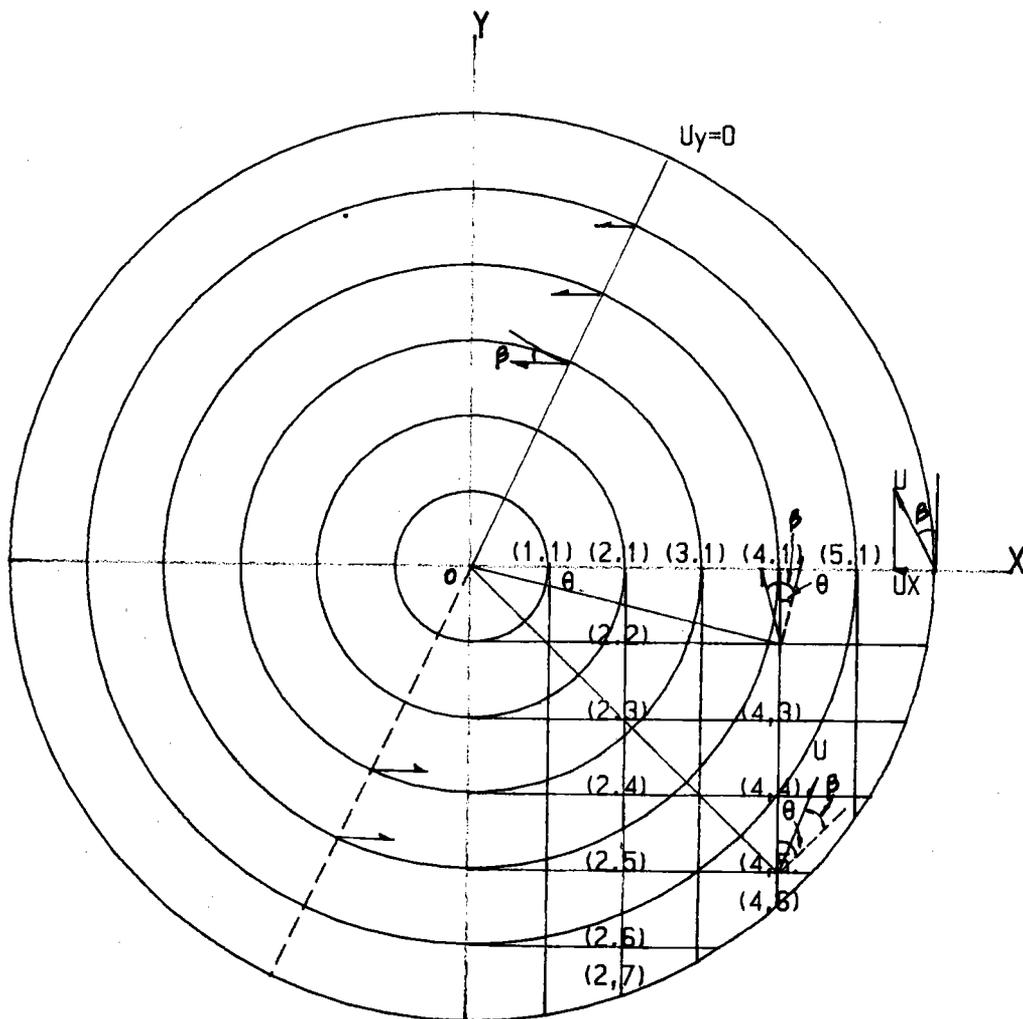
$$\frac{gH_y}{UU_y} = A_1 \tanh[B_1 \left( \frac{gF_y}{UU_y} \right)^{m_1}]$$

$$F_y = \frac{UU_y}{g} \left( \frac{1}{B_1} \tanh^{-1} \left( \frac{1}{A_1} \left( \frac{gH_y}{UU_y} \right) \right) \right)^{\frac{1}{m_1}}$$

$$U_x = U \cos(90^\circ - \beta)$$

$$U_y = U \cos(\beta - \theta)$$

$$H_s^2 = H_x^2 + H_y^2$$



#### 4. 推算結果

表 5 - 1 是採用數個  $\frac{fR}{U_R}$  值不同的模式颶風依 Bretschneider 法推算和用等效風域法推算所得之最大風速半徑 R 處之代表波高， $H_R^*_{COMP}$  代表 Bretschneider 法推算之數值（以下簡稱 B 法）， $HH_R$  則代表等效風域推算之結果，大致來說，本法推算之數值較  $H_R^*_{COMP}$  略小，約為  $H_R^*_{COMP}$  之 80 ~ 90 %，且由表中可看出，當  $\frac{fR}{U_R}$  值較小時，兩者較為接近， $\frac{fR}{U_R}$  值變大時，兩數值之差異亦增大。

其次在全風場內波高分佈的比較可由圖 5 - 4 和圖 5 - 5 看出，圖 5 - 4 為 B 法所得之  $H_r/H_R$  對應  $r/R$  圖，圖 5 - 5 則為等效風域法所得之結果，兩圖之趨勢相同，但同一個  $\frac{fR}{U_R}$  值之綫，等效風域法之結果，位置均較 B 法為低，且在  $r/R = 2$  處，B 法有向上凸起之最大值，等效風域法則無此現象。

為驗證等效風域法在實際颶風波浪推算上之效果，我們選擇了數個侵襲台灣之颶風加以推算，其路徑見圖 5 - 6，其中薇拉颶風於 7 月 31 日 7 點 30 分登陸基隆，中心氣壓為 930 mb，R 值經推定為 16 n.m.，移動速度為 12 節，實測波浪資料係取自位於八尺門之壓力式波高計（水深 125 呎），由於水深與波長之比值為淺水波性質，故推算之結果應乘以淺化係數  $K_s$  加以修正，首先假定薇拉颶風處於穩定之狀態，利用等效風域法推算之波浪場如圖 5 - 7 所示，其中左半圓係以一米為間隔，繪出波高同心圓，右半側則以 R 處之波高為 100 %，而繪出百分比同心圓，這個結果再配合颶風之移動效應可推得移動颶風之波浪場，結果見表 5 - 2，表中  $HH_r$  為穩定之颶風狀態應有之波高， $HH_a$  為已考慮移動效應後之代表波高， $HH_{K_s}$  則為再經過淺化係數  $K_s$  修正（ $\times 0.913$ ）後之數值。圖 5 - 8 為八尺門波浪測站實測資料與推算值之比較，在颶風接近期間，等效風域法之推算值最接近實測值，兩者幾乎重合，1630 至 1810 這段時間，測站位於颶風最大風速半徑 R 內，無論是 Bretschneider 法或等效風域法均無法預測波高狀況，至於實測資料則顯示最大代表波高為 40.9 呎，在颶風離去期間，圖上顯示推算值均大於實測值，此現象事實上相當合理，因颶風登陸後風場結構已受破壞，且測站位于陸地邊緣，風域受到陸地限制顯著變小，故以穩定颶風為基本架構而推算之波浪自然應當偏大。

至於另外兩個颱風 NINA 及 BRENDA 之推算結果並不理想（參見圖 5—9 及圖 5—10）以 NINA 颱風而論，B 法及等效風域法推算值均較實測值為大。由於實測資料係取自於其它論文所載，測站之位置與水深等特性是否有特殊之處，有待查考，單以推算結果而言 B 法之誤差較大。至於 BRENDA 颱風則等效風域及 B 法推算值均遠低於實測值。且等效風域法數值最低。由圖 5—6 可看出 BRENDA 颱風之路徑係於距測站相當距離外掠過，因此波高成份中必有相當大之湧浪在內，相信這是實測波高偏大之主要因素。

$N_0$	$\frac{f_R}{U_R}$	緯度 $\phi$	$f=0.525$ $\times \sin \phi$	$R$ ( $nm$ )	$U_R$ ( $knots$ )	$K$	$\Delta P$ ( $IN. HG$ )	$RAP$	$K'$	$H_R^* = \frac{H_R}{K' \sqrt{RAP}}$	$H_R^*_{COMP}$ ( $M.$ )	$HH_R$ ( $M.$ )	$\frac{HH_R}{H_R^*_{COMP}}$
2	0.0	0°	0.0	10	110.7	70	2.5	25	7.50	11.4	11.1	10.0	0.90
3	0.0	0°	0.0	25	99.0	70	2.0	50	7.50	16.1	14.0	12.4	0.88
6	0.025	30°	0.2625	10	104.1	66.0	2.55	25.5	6.54	10.1	10.4	8.7	0.83
7	0.025	22°	0.2009	14	112.3	67.0	2.88	40.3	6.55	12.6	13.0	10.9	0.84
8	0.025	11°	0.1002	25	102.4	68.5	2.29	57.3	6.56	15.1	14.3	12.2	0.85
10	0.05	28°	0.2465	15	74.6	67	1.3	19.5	5.81	7.8	7.6	6.5	0.86
11	0.05	22°	0.1967	20	80.1	67	1.5	30.0	5.85	9.8	9.7	8.0	0.83
15	0.10	22°	0.1967	40	80.0	67	1.57	62.8	5.01	12.1	11.9	9.8	0.83
20	0.15	35°	0.3011	35	70.0	66	1.30	45.5	4.50	9.3	9.4	7.6	0.81
24	0.20	35°	0.3011	40	60.0	66	1.00	40.0	4.10	7.9	7.9	6.4	0.81
26	0.20	41°	0.3444	40	67.5	63.8	1.36	54.4	4.10	9.3	9.3	7.4	0.80
39	0.30	35°	0.3011	65	64.9	66.0	1.28	83.2	3.55	9.8	10.0	8.1	0.81

表 5-1 以 Bretschneider 法及等效風域法推算穩定颱風  
最大風速半徑 R 處之代表波高之比較

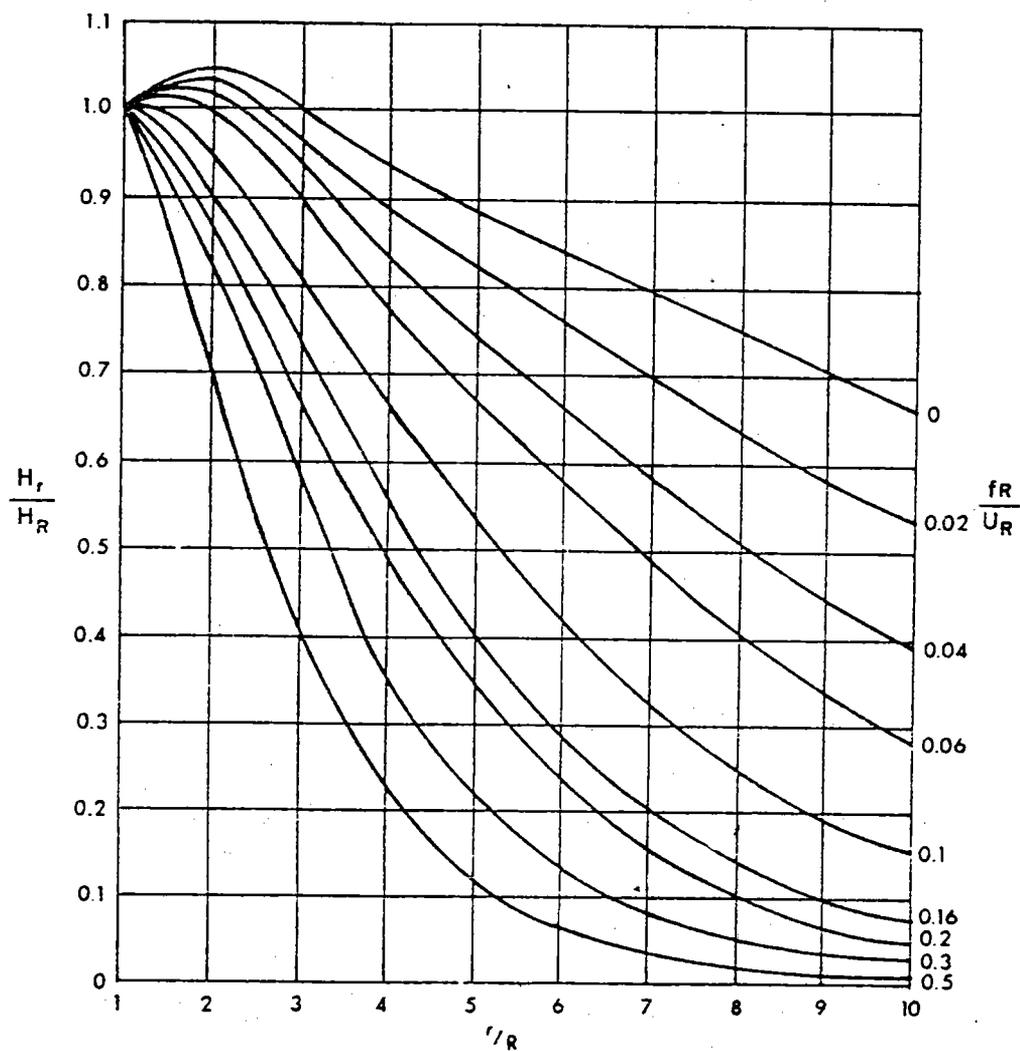


圖 5 - 4 以 *Bret* 法推算不同  $\frac{fR}{U_R}$  值之颱風波浪場之分佈

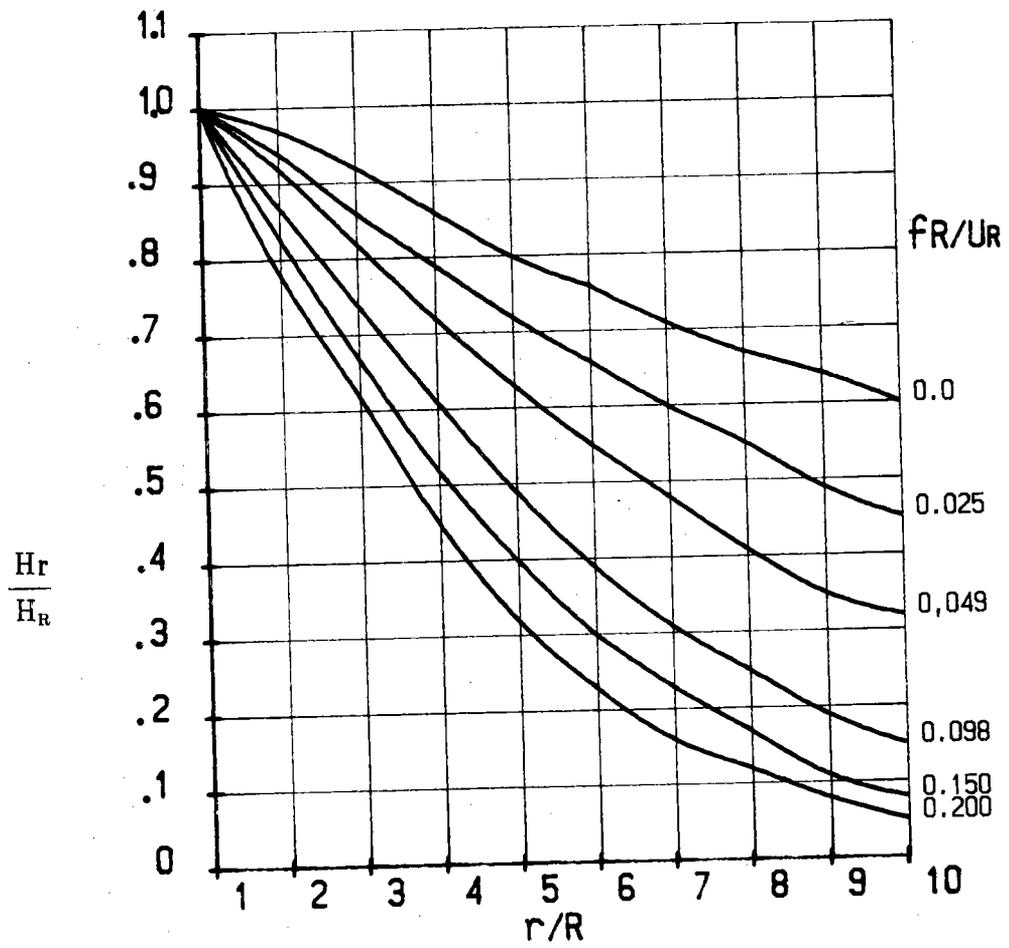


圖 5 - 5 以等效風域法推算不同  $\frac{fR}{U_R}$  值之

颱風波浪場之分析

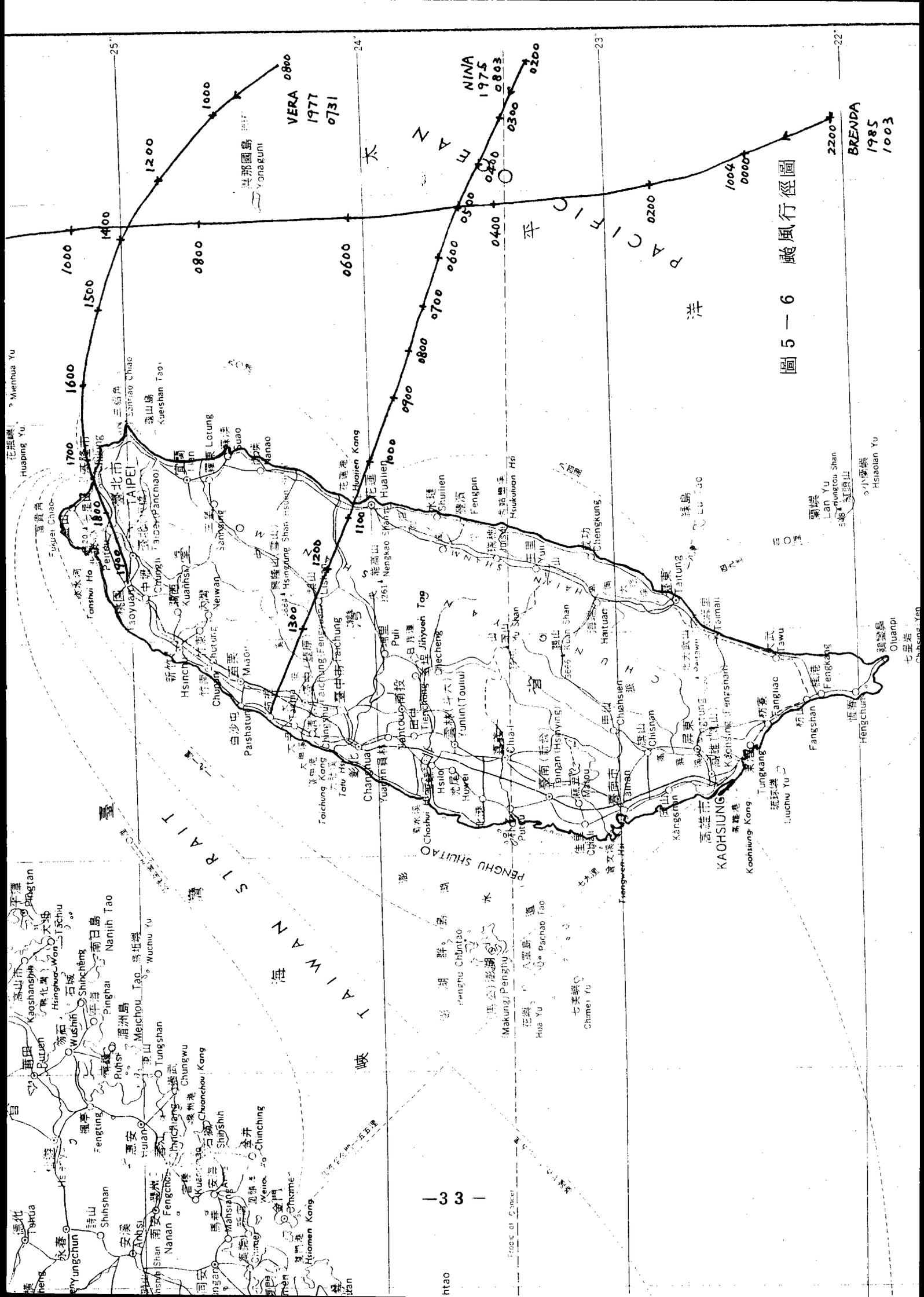


圖 5-6 颱風行徑圖

LOCAL TIME	氣壓 (mb)	$\theta^\circ$	$\cos(\theta+\beta)$	$V_s$ (knots)	DR (n. m.)	DR/R	$\Delta U$	$\frac{\Delta U}{(1+\frac{U_R}{S})^2}$	HHr (M.)	HHa (M.)	HHks (M.)
7/31 11	930	115	-0.77	10	86	5.37	-3.85	0.85	6.5	5.5	5.02
12	930	110	-0.71	10	76	4.75	-3.55	0.87	6.9	6.0	5.5
13	930	100	-0.57	10	68	4.25	-2.85	0.91	7.3	6.6	6.1
14	930	100	-0.57	12	58	3.63	-3.42	0.90	7.9	7.1	6.5
15	930	98	-0.54	12	42	2.63	-3.24	0.92	8.8	8.1	7.4
16	930	95	-0.5	12	24	1.5	-3.0	0.93	9.6	8.9	8.1
17	930	90	-0.42	12	78	0.5	-	-	-	-	-
18	935	270	0.42	11	78	0.5	-	-	-	-	-
19	940	270	0.42	11	21	1.31	2.3	1.05	9.4	9.8	8.9
20	950	285	0.64	11	38	2.4	3.5	1.1	8.6	9.4	8.6

表 5-2 薇拉 (VERA) 颱風通過期間，八尺門測站代表波高推算表

註： $\beta=25^\circ$   $\theta$  為測站之位置角，如以 Y 軸表颱風行進方向， $\theta$  角為由 X 軸

開始反時針計算

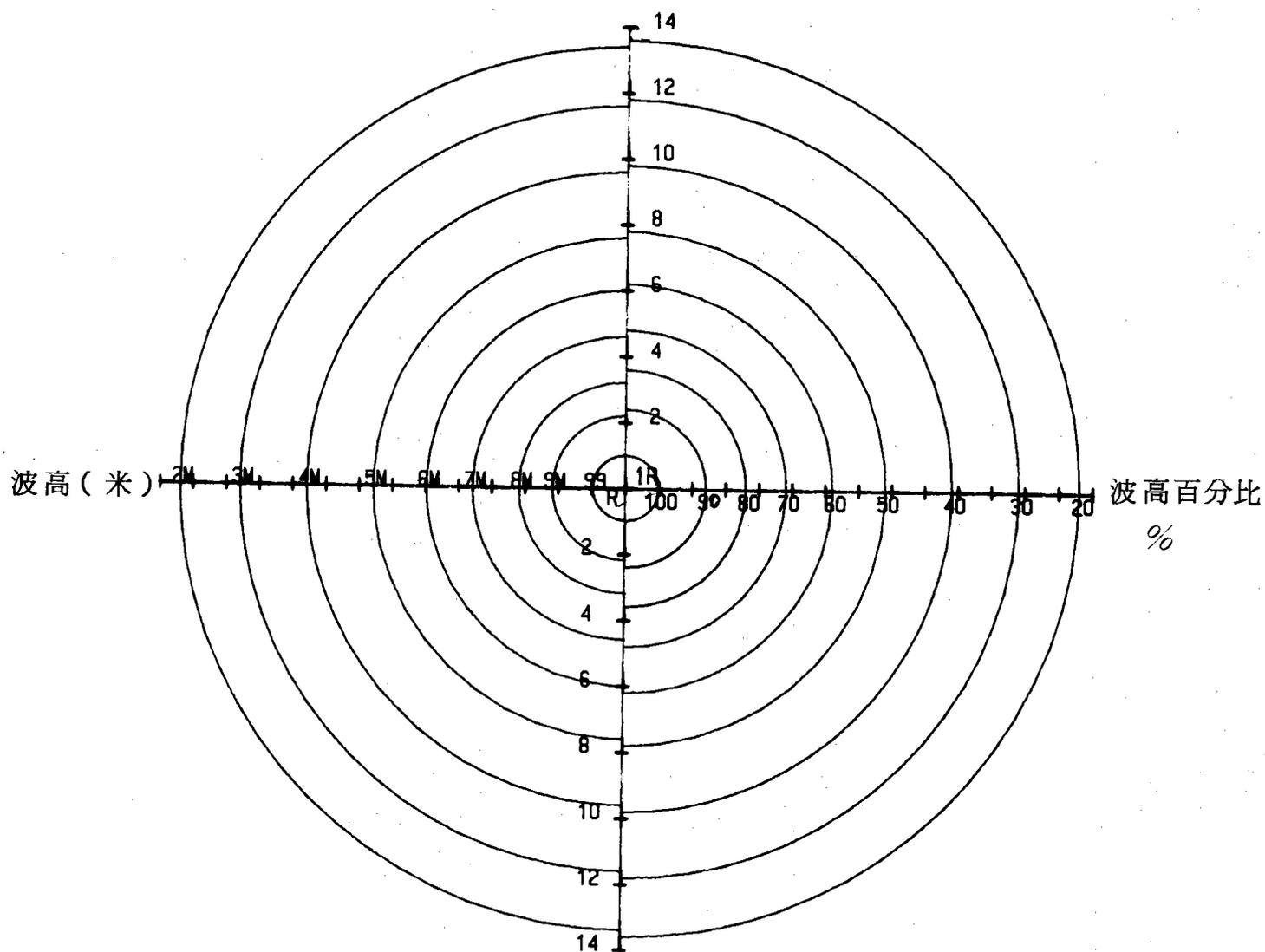


圖 5 - 7 以等效風域法推得 VERA 颱風之波浪場

註：假設為穩定狀態

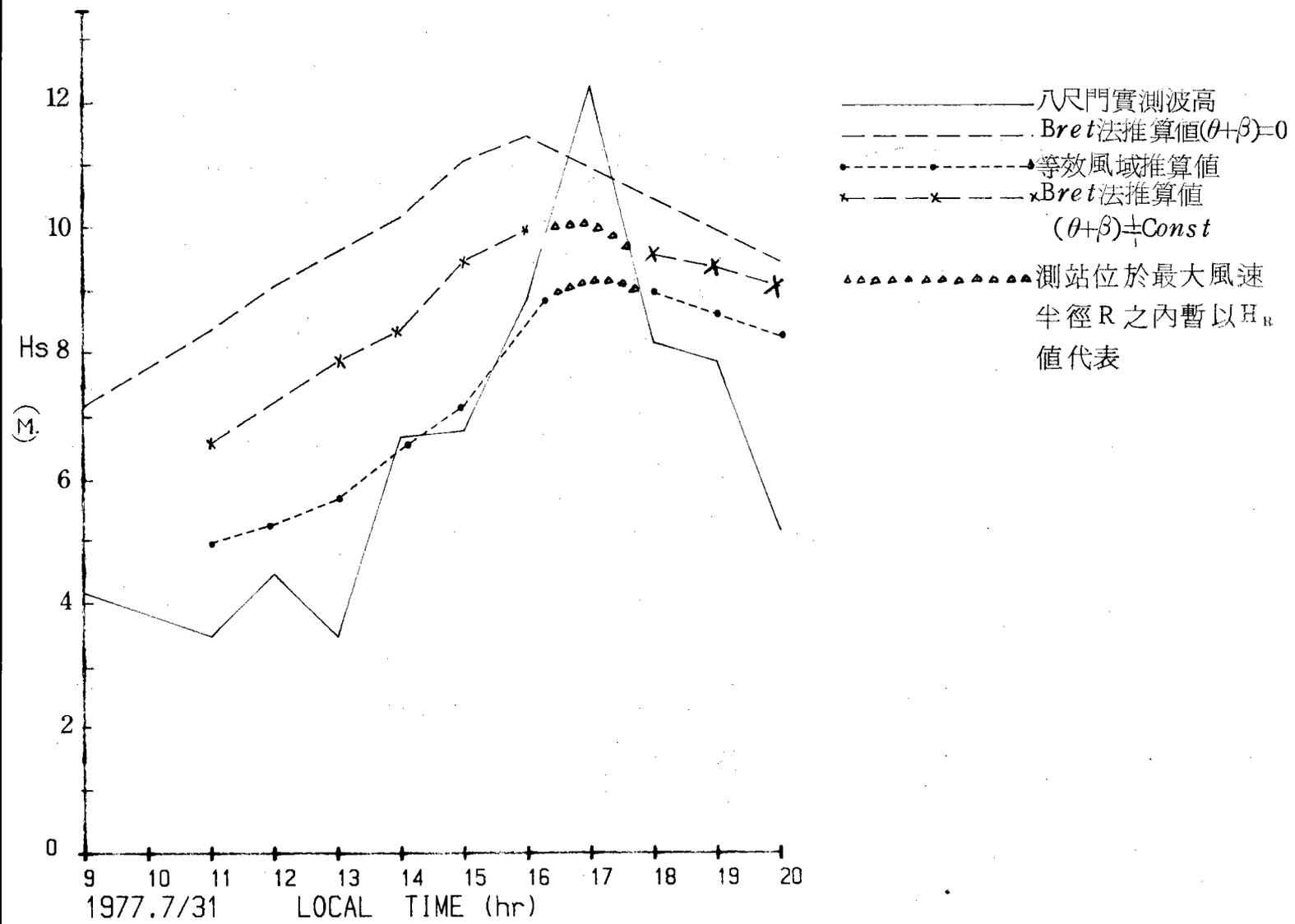


圖 5 - 8 薇拉颱風實測與推算代表波高之比較

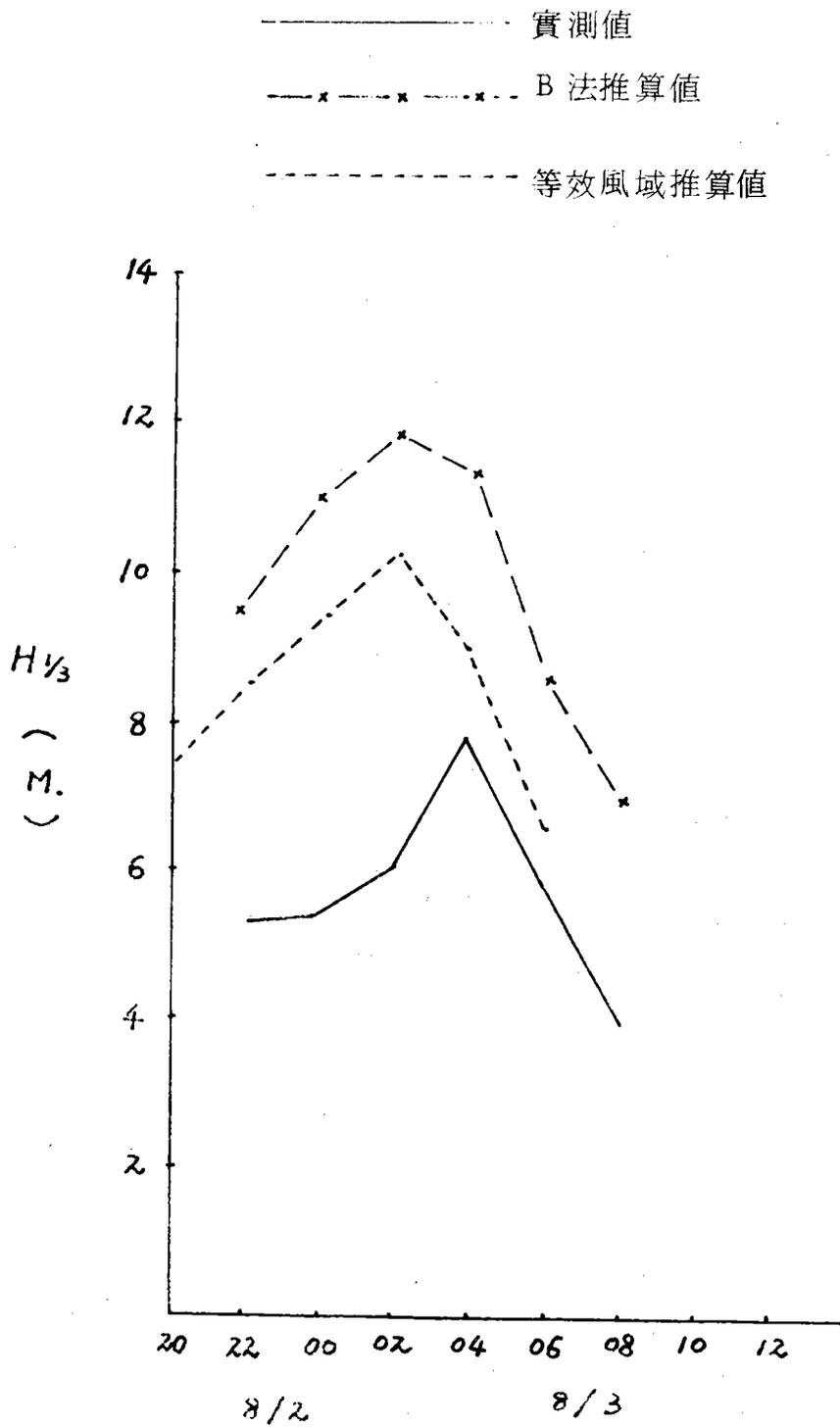


圖 5 - 9 NINA 颱風實測與推算代表波高之比較

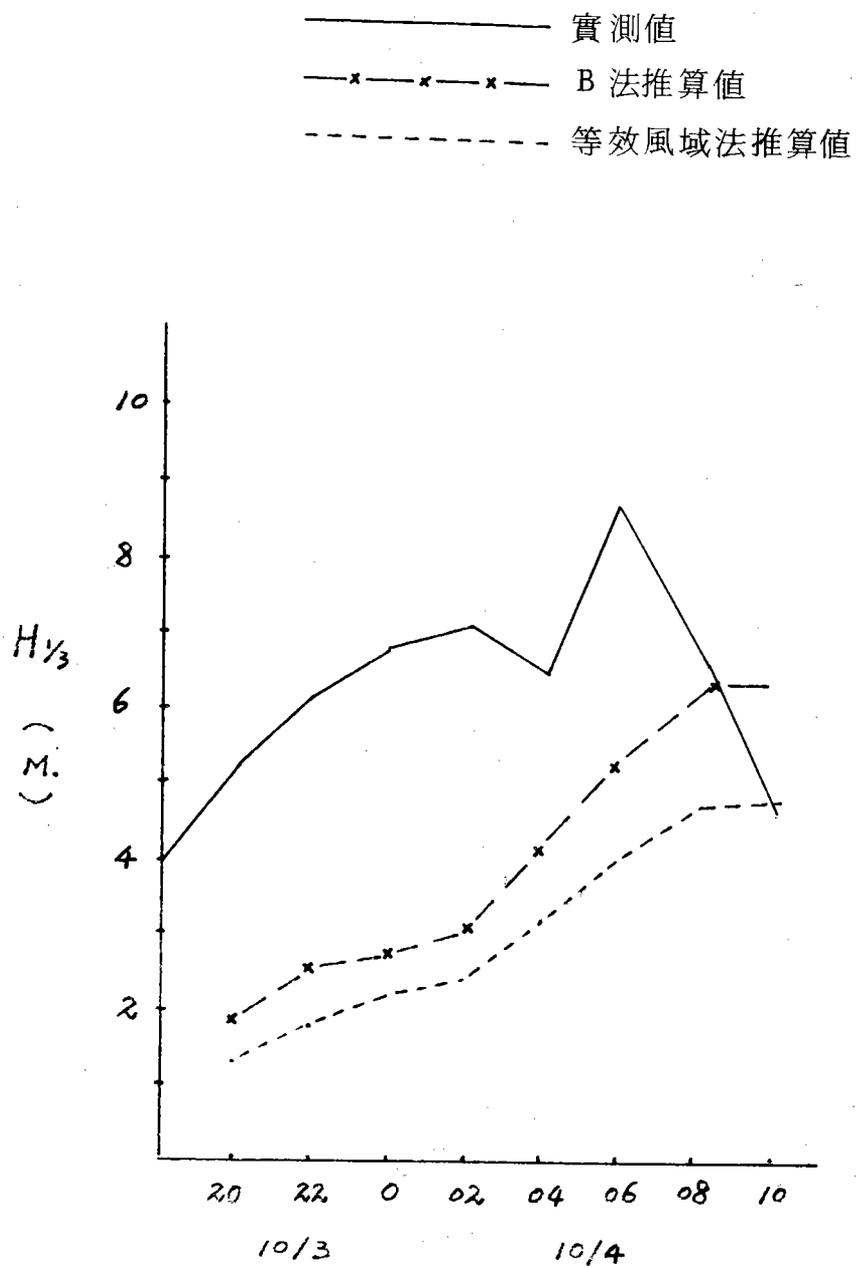


圖 5 - 10 BRENDA 颱風實測與推算代表波高之比較

## 5. 結論：

- (1) 以等效風域法推算颱風場內最大風速半徑  $R$  處之代表波高，與  $B$  法之結果相似，而數值約為  $B$  法所得之  $85\%$ 。
- (2) 就整個風域內波浪之分佈情形而論，等效風域法在不同之  $r/R$  處， $H_r / H_R$  比值亦較  $B$  法為低， $fR / U_R$  值較小時，偏差較大，且在  $r/R = 2$  時未有  $B$  法之凸起現象。
- (3) 與薇拉颱風之實測資料比較，等效風域法在  $R$  處以外的結果均相當符合，但  $R$  以內之情況無法推算，至於  $NINA$  颱風及  $BRENDA$  颱風則推算結果較不理想。
- (4) 本文僅以數個颱風之實測資料比對，在統計學上尚難論斷等效風域法之準確性，爾後應繼續配合其它實測颱風資料加以驗證。並針對颱風之特性，如強度、暴風半徑大小、路徑、行進速度等多加統計與分析，以求得更有系統的結果。

## 六、結論與建議

梁 乃 匡

1. 由中央氣象局所提供的風場及波浪資料所求出的風能授受系數  $\xi$ ，四個測站分別是鼻頭角  $2.9E - 05$ ，東吉島  $2.4E - 05$ ，小琉球  $0.96E - 05$ ，新港  $2.6E - 05$ 。

由這些經驗常數所決定的模式推算出來的波浪與實測比較，波高除了新港與鼻頭角有稍偏大外，東吉島與小琉球皆很脛合，大致而言推算結果相當理想。但尚需調整風場模式，以求出最佳授受係數  $\xi$ 。

2. 經驗常數應為季節的函數，因此需要更多的風場資料與波浪資料來求常數群。
3.  $T^{1/3}/U_{RS}$  與  $DD/T_R^2$  為最佳的推算颱風湧浪週期的參數，由目前的資料，湧浪週期推算公式為

$$\frac{T^{1/3}}{U_{RS}} = 0.2 + 0.023 \frac{DD}{T_R^2} - 0.0005 \frac{(DD)^2}{T_R^4}, \quad \frac{DD}{T_R^2} \leq 20$$
$$\frac{T^{1/3}}{U_{RS}} = 0.46 \quad \frac{DD}{T_R^2} > 20$$

4. 推測湧浪可能與當地風浪混在一起，而使  $T^{1/3}$  變小，所以應當由波譜求出湧浪週期取代  $T^{1/3}$ 。
5. 由等效風域法求出的颱風波浪場與 *Bretschneider* 原來所提出者有異，何者較為正確，應繼續以實測值來比較。

## 七、參考文獻

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Bretschneider, C.L., Tamage, E.E. (1976), Hurricane Wind and wave forecasting techniques, proceedings 15th International coastal Engineering conference, PP. 202-237.

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附錄 I 波浪預報程式

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15-JUN-1987 04:19

PAGE 1

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CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C
C THIS PROGRAM IS FORECASTING WAVE AROUND TAIWAN C
C SUPPORT BY C.M.B SET UP BY C.C-CHIEN 1987/06/04 C
C CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
CHARACTER#12 TYNAME(4)
CHARACTER#2 PA

```

```

C WIND DATA
C DIMENSION WS(150,800),WD(150,800),WLDN(150),WLAT(150)
C DIMENSION IY(800),IM(800),ID(800),IH(800)

```

```

C TYPHCON DATA
C DIMENSION IY(4,120),ITH(4,120),ITD(4,120),ITH(4,120)
C DIMENSION TLAT(4,120),TLON(4,120),FO(4,120),VF(4,120),R(4,120)

```

```

C MONSOON WAVE
C DIMENSION HM(100,80),PM(100,80)

```

```

C TYPHCON WAVE
C DIMENSION HT(4,120,100),PT(4,120,100)
C DIMENSION KY(4,120,100),KTH(4,120,100)
C DIMENSION KKTH(4,120,100),TLAG(4,120,100)

```

```

C WAVE GRID POSITION & CONSTANTS
C DIMENSION GLON(100),GLAT(100),CURSI(100),CO(100,4)

```

```

C OTHERS
C DIMENSION FAC(5),LL(4)

```

```

C LAND DATA
C DIMENSION XL(500),YL(500),XX(200),YU(200),YD(200)
C DIMENSION YY(200),XU(200),XD(200)

```

```

C OUTPUT DATA
C DIMENSION H(100),T(100),WAVDIR(100)

```

C TOTAL DIMENSION = 646069

C OPEN INPUT DATA FILE

```

C OPEN(UNIT=10,FILE='MONSOON.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=21,FILE='TYPH1.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=22,FILE='TYPH2.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=23,FILE='TYPH3.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=24,FILE='TYPH4.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=30,FILE='GRID.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=41,FILE='LAND.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=42,FILE='XLAND.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=43,FILE='YLAND.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=50,FILE='INDBEL.DAT',FORM='FORMATTED',STATUS='OLD')
C OPEN(UNIT=70,FILE='TEST.DAT',FORM='FORMATTED',STATUS='NEW')

```

C READ IN WIND DATA , L IS DATA BLOCK NO.  
 C WIND FIELD GRID NO. I=150

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15-JUN-1967 04:19

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```

C
C      WS = WIND SPEED
C      WD = WIND DIRECTION
C
19  L=1
50  READ(10,11,END=19)IY(L),IM(L),ID(L),IH(L)
11  FORMAT(4(IX,I2))
    DO 90 I=1,150
90  READ(10,12,END=19)WS(I,L),WD(I,L)
12  FORMAT(2(4X,F6.2))
    L=L+1
    GO TO 50

```

```

C      READ IN TYPHOON DATA
C      LL(I) IS DATA BLOCK NO. OF
C      TYPHOON(I), I=1,2,3,4

```

```

19  L=L-1
    LL1=1
    WRITE(5,8001)L
8001 FORMAT(5X,'8001',2X,'L=',I5)
    READ(21,13,END=29)TYNAME(1)
13  FORMAT(A12)
61  READ(21,11,END=29)IY(1,LL1),ITH(1,LL1),ITD(1,LL1),ITH(1,LL1)
    - ,R(1,LL1)
25  FORMAT(2(1X,F7.2),3(1X,F7.1))
    LL1=LL1+1
    GO TO 61
29  LL2=1
62  READ(22,13,END=39)TYNAME(2)
    READ(22,11,END=39)IY(2,LL2),ITH(2,LL2),ITD(2,LL2),ITH(2,LL2)
    READ(22,25,END=39)TLAT(2,LL2),TLON(2,LL2),PO(2,LL2),VF(2,LL2)
    - ,R(2,LL2)
    LL2=LL2+1
    GO TO 62
39  LL3=1
63  READ(23,13,END=49)TYNAME(3)
    READ(23,11,END=49)IY(3,LL3),ITH(3,LL3),ITD(3,LL3),ITH(3,LL3)
    READ(23,25,END=49)TLAT(3,LL3),TLON(3,LL3),PO(3,LL3),VF(3,LL3)
    - ,R(3,LL3)
    LL3=LL3+1
    GO TO 63
49  LL4=1
64  READ(24,13,END=59)TYNAME(4)
    READ(24,11,END=59)IY(4,LL4),ITH(4,LL4),ITD(4,LL4),ITH(4,LL4)
    READ(24,25,END=59)TLAT(4,LL4),TLON(4,LL4),PO(4,LL4),VF(4,LL4)
    - ,R(4,LL4)
    LL4=LL4+1
    GO TO 64

```

H-2

```

C      READ IN WIND AND WAVE GRID POSITION & CONSTANT DATA
C      WIND GRID NO. I=150
C      COORDINATE X=WLON(I) Y=WLAT(I)
C      WAVE GRID NO. K=89
C      COORDINATE X=GLON(K) Y=GLAT(K)
C      CURSI(K),CO(K,J) J=1,2,3,4 ARE CONSTANTS

```



15-JUN-1987 04:19

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```

READ(30,113)WLGK(I),WLAT(I)
WRITE(5,113)WLGK(I),WLAT(I)
103 FORMAT(10X,F7.3,5X,F7.3)
113 DO 104 K=1,89
READ(30,114)GLON(K),GLAT(K),CURSI(K),CO(K,1),CO(K,2),CO(K,3),
-CO(K,4)
104 WRITE(5,114)GLON(K),GLAT(K),CURSI(K),CO(K,1),CO(K,2),CO(K,3),
-CO(K,4)
114 FORMAT(10X,F7.3,5X,F7.3,5(2X,E8.2))
C WRITE(5,8020)J,I,WLON(I),WLAT(I),GLON(I),GLAT(I)
C READ IN LAND,XLAND,YLAND,DAY LAND DATA NO. = IA
C XLAND DATA NO. = IB
C YLAND DATA NO. = IC
C
IA=1
3012 READ(41,3011,END=3050)XL(IA),YL(IA),ICODE
3011 FORMAT(1X,F6.2,2X,F6.2,2X,I2)
IF(ICODE.EQ.99) GO TO 3050
IA=IA+1
GO TO 3012
C
C READ XLAND DATA
C
IB=1
3020 READ(42,3021,END=3060)XX(IB),YU(IB),YD(IB),ICODE
3021 FORMAT(1X,F6.2,2X,F6.2,2X,F6.2,2X,I2)
IF(ICODE.EQ.99) GO TO 3060
IB=IB+1
GO TO 3022
C
C READ YLAND DATA
C
IC=1
3060 READ(43,3021,END=3070)YY(IC),XU(IC),YD(IC),ICODE
3032 IF(ICODE.EQ.99) GO TO 3070
IC=IC+1
GO TO 3032
C
C CHECK THE WIND DATA LENGTH (=L)
3070 IF(L.LT.40) GO TO 333
C
C ENTER THE CURRENT TIME INCLUDE (YEAR,MONTH,DAY,HOUR)
C
WRITE(5,1)
9 FORMAT(/,5X,'ENTER THE CURRENT TIME ,YEAR,MONTH,DAY,HOUR 412 ','$)
1 READ(5,2)IYC,IMC,IOC,IMC
2 FORMAT(4I2)
3 FORMAT(/,5X,'YEAR=',I2,3X,'MONTH=',I2,3X,'DAY=',I2,3X,'HOUR=',I2)
4 WRITE(5,4)
4 FORMAT(/,5X,'CURRENT TIME IS CORRECT ? (YE.OR.NO)','$)
5 READ(5,5)PA
5 FORMAT(A2)
IF(PA.EC.'YE') GO TO 70
GO TO 9

```

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, SO WE HAVE 8 DATUM IN ONE DAY J

DO 152 N=1,40  
M=M+1  
IYM=IY(M)  
IMM=IM(M)  
IDM=ID(M)  
IHM=IH(M)

TRANSFER WIND DATA TIME TO ABS. TIME

CALL TRTIME(CYP, IMM, IDM, IHM, IABSYM, IABSHM, 1)  
LL(1)=LL1  
LL(2)=LL2  
LL(3)=LL3  
LL(4)=LL4

CHECK IN THIS WIND DATA STEP THE ABS. TIME SUPERPOSITION  
TYPHOON DATA ABS. TIME

YE --> IF THESE POINTS INNER 10R (GO TO SUBROUTINE SUBT)  
CHANGE THE WSC(I,L)=0.  
NO --> NO CHANGE

DO 107 IPI=1,4  
KE=LL(IPI)  
DO 105 KPK=1,KE  
ITYI=ITY(IPI, KPK)  
ITMI=ITM(IPI, KPK)  
ITDI=ITD(IPI, KPK)  
ITHI=ITH(IPI, KPK)

TRANSFER TYPHOON DATA TO ABS. TIME IN THIS STEP

CALL TRTIME(CIYI, ITMI, ITDI, ITHI, IABSYI, IABSHI, 1)  
IF(IABSHM.EQ.IABSHI) GO TO 115  
CONTINUE  
CALL SUBT(CPI, KPK, M, TLAT, TLON, PD, VF, R, MS, WLDN, WLAT)  
CONTINUE

CONSIDER 150 POINTS OF WIND FILED

DO 154 I=1,150  
XM=WLDN(I)  
YM=WLAT(I)  
XA=GLON(J)  
YA=GLAT(J)

WRITE(5,8020)J,I, XM, YM, XA, YA  
FORMAT(5X, J=1, I4, ' I=', I4, ' XM=', F7.3, ' YM=', F7.3, ' XA=', F7.3,  
-1, YA=', F7.3)

CALL DISC(XA, YA, XM, YM, RR)  
CALL ANGCXM, YM, XA, YA, CD, IEEP)  
DA=2\*3.14159\*6366.71\*2.\*ABS(COSD(90.5-YA)-COSD(89.5-YA))/360.  
IFCF.LE.RR) F=RR

IF(IEER.EQ.1) GO TO 154  
RLU=0.5\*WSC(I, M)\*(TI+(41-N)\*DT)\*3.6  
RL=0.5\*WSC(I, M)\*(TI+(40-N)\*DT)\*3.6  
BETA=ABS(CO-WDCI, M)  
ZETA=BETA\*GT.180.) BETA=360.-BETA

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C      IF(BETA-GE.90.) GO TO 154
C      CONSIDER SHELTERING EFFECT JEER = 1 SHELTERING OCCURRED
C      JEER = 0 SHELTERING NO HAPPENED
C      CALL SHEL(XM,YM,XA,YA,XX,YU,YY,XC,XU,XD,XL,YL,JEER
- ,IA,IB,IC)
C      IF(ABS(JEER-1).LE.0.005) GO TO 154
C      COUNT=CCOUNT+1
C      WRITE(5,8005)RL,RR
C8005  FORMAT(5X,'RL=',F8.2,' RR=',F8.2)
C      CALL EAREACRR,RL,LL,DA,CD)
C      IF(CDA-LT.0.0005) GO TO 154
C      WRITE(5,8008)
C8008  FORMAT(5X,'STEP 4')
C      SUUBA=WSCI,M)*WSCI,M)*COSD(BETA)*EXP(-0.08*RR/(WSCI,M)
- *WS(I,M)))/DA/RR
C      SMUDR=SMUDR+WSCI,M)
C      SMDR=SMDR+1
C      SUMSK=SUMSK+SUUBA*WSCI,M)
C      SUUBE=SUUBE+SUUBA
C      DELT=TI+(40-N)/OT
C      IF(CUR.LE.OELT) DUR=DELT
C      CONTINUE
C      CONTINUE
154  IF(SUUB8-EC.0.) GO TO 335
152  IF(SMUR.LE.0.) GO TO 335
      AA=2.*3.14159/9.8
      WAVDIR(J)=SUMSK/SUUBE
      TOUR=TI+OUR
      UMEAN=SMUDR/SMUR
      TSF=AA*UMEAN*((9800.*F/UMEAN**2.)*CD(J,1)+CD(J,2))
      TSD=AA*UMEAN*((35280.*TCUR/UMEAN)*CD(J,3)+CD(J,4))
      HSF=SQRT(CURSI(J)*0.82*SUUBE/TSF)
      HSD=SQRT(CURSI(J)*0.82*SUUBE/TSD)
      GO TO 159
335  TSF=0.0
      TSD=0.0
      HSF=0.0
      HSD=0.0
C      OUTPUT RESULT IYO,IMO,IOO,IHO
C      J,XA,YA,HSD,TSD,HSF,TSF,WAVDIR(J),COUNT
159  HM(J,NDN)=HSF
      PM(J,NDN)=TSD
      WRITE(5,8030)HSF,TSF,HSD,TSD,UPEAN
6030  FORMAT(5X,'HSF=',F7.2,' TSF=',F7.2,' HSD=',F7.2,' TSD=',F7.2,
- , UME=',E8.2)
C      WAVDIR(J),IABSYC,IABSHC)=WAVDIR(J)
150  CONTINUE
      KK=KK+1
      IABSHC=IABSHC+3
      NON=NON+1
      WRITE(5,8003)KK,NDN,L
8003  FORMAT(5X,'8003', ' KK=',I5,' NON=',I5,' L=',I5)
      IF(KK-GE.L) GO TO 2000
      GO TO 171

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15-JUN-1987 04:19

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2000 CALL TYPHOON(LL,TLAT,TLON,PD,VF,R,ITY,ITM,ITD,ITH,KTY,KTH,HT,PT,
      -KKTH,ILAG,XX,YU,YD,YY,XU,XD,XL,YL,IA,IB,IC,GLON,GLAT)
      DO 8200 N=1,3
      DO 8250 I=1,8
      DO 8300 J=1,89
      WRITE(70,71)N,I,J,HTCN,I,J,PT(N,I,J)
      FORMAT(5X,'N=',I4,' I=',I4,' J=',I4,' HT=',F7.2,' PT = ',F7.2)

```

```

71 CONTINUE
8300 CONTINUE
8250 CONTINUE
8200 CONTINUE
      CALL MPTWV(LL,KTY,KTH,HT,ILAG)

```

C RESET WAVE HEIGHT & PERIOD DISTRIBUTE

```

C
C CALL TRIME(IYC,IMC,IOC,IHC,IABSYC,IABSHC,I)
      ICY=IABSYC
      ICH=IABSHC
      FAC(1)=0.33333
      FAC(2)=0.66667
      FAC(3)=1.
      FAC(4)=0.66667
      FAC(5)=0.33333
      NO=1

```

1234

```

      DO 100 J=1,89
      SUMH=HM(J,NO)
      SUMT=PM(J,NO)
      K=1

```

C FOR MONSOON WAVE

```

C
C DO 200 LP=NO-2,NO+2
      IF(LP.LE.0) GO TO 202
      IF(LP.GT.NO) GO TO 202
      THM=CHM(J,LP)*2.*FAC(K)
      SUMH=SUMH+THM
      SUMT=SUMT+THM*PM(J,LP)
      K=K+1
      CONTINUE
C202
C200 CONTINUE
C

```

C FOR TYPHOON WAVE

```

C
C ICOUNT=0
      DO 300 N=1,4
      KE=LL(N)
      DO 400 I=2,KE
      IF(KTY(N,I,J).NE.ICY) GO TO 300
      IDH=ABS(ICH-KTH(N,I,J))
      IF(IDH.GE.3) GO TO 400
      ICOUNT=ICOUNT+1
      KK=3-IDH
      THT=(HTCN,I,J)*2.*FAC(KK)
      SUMH=SUMH+THT
      SUMT=SUMT+THT*PT(N,I,J)
      CONTINUE
      ICOUNT=ICOUNT+1
      IF(ICOUNT.EQ.0) GO TO 301
      HC(J)=SQRT(SUMH)

```

400  
300



```

      T(J)=0.
    ELSE
      T(J)=SUMT/SUMH

END IF
GO TO 100
301 H(J)=SUMH
100 T(J)=SUMT
CONTINUE
CALL TRTIME(IC,IMC,ICG,IMD,ICY,ICH,-1)
WRITE(50,5001)IYD,IMO,I00,IMO
FORMAT(/5X,'YEAR=',I3,3X,'MONTH=',I3,3X,'DAY=',I3,3X,'HOUR=',
-,I3,3X)
DO 5005 I=1,89
5005 WRITE(50,5002)I,H(I),T(I)
5002 FORMAT(5X,'POINT NO =',I3,3X,'M13=',F7.2,3X,'T13=',F7.2)
      KL=KL+1
      ICH=ICH+3
      IF(KL.GE.L) GO TO 9999
      NO=NO+1
      GO TO 1234
333 WRITE(5,3331)
GO TO 9999
3331 FORMAT(5X,'ERROR')
334 WRITE(5,3331)
GO TO 9999
336 WRITE(5,3331)
GO TO 9999
337 WRITE(5,3331)
GO TO 9999
9999 CLOSE(UNIT=10)
CLOSE(UNIT=21)
CLOSE(UNIT=22)
CLOSE(UNIT=23)
CLOSE(UNIT=24)
CLOSE(UNIT=30)
CLOSE(UNIT=41)
CLOSE(UNIT=42)
CLOSE(UNIT=43)
CLOSE(UNIT=50)
CLOSE(UNIT=70)
STOP
END
SUBROUTINE TYPHOON(LL,TLAT,TLON,PC,VF,RPR,ITY,ITM,ITD,ITH,KTY,
-KTH,HT,PT,KKTH,TLAG,XX,YU,YD,YY,XU,XD,XL,YL,IA,IB,IC,GLON,GLAT)
CHARACTER*5 NAME
DIMENSION LL(4),TLAT(4,120),TLON(4,120),PC(4,120),VF(4,120)
DIMENSION RPR(4,120),ITY(4,120),ITM(4,120),ITD(4,120),ITH(4,120)
DIMENSION GLON(100),GLAT(100)
DIMENSION KTY(4,120,100),KTH(4,120,100),HT(4,120,100)
DIMENSION PT(4,120,100),KKTH(4,120,100),TLAG(4,120,100)
DIMENSION XL(500),YL(500),XX(200),YU(200),XD(200)
DIMENSION YD(200),XU(200),XD(200)
DO 100 N=1,4
L=LL(N)
DO 200 I=1,L
XJ=JLON(N,I)
YI=TLAT(N,I)
IF(I+1).GE.L) GO TO 100

```



15 JUN 1987 04:19

-OJAI:TCCHIEN.CWB3WAVET2.FOR;6

```

X2=TLON(N,I+1)
Y2=TLAT(N,I+1)
DO 300 J=1,89
XM=GLON(J)
YM=GLAT(J)
CALL SHEL1(X1,Y1,XM,YM,XX,YY,XY,XU,XD,XL,YL,JEER,IA,IB,IC)
IF(ABS(JEER-1).LE.0.005) GO TO 300
CALL DIS(X1,Y1,XM,YM,AM)
CALL DIS(X1,Y1,X2,Y2,AB)
CALL ANGLECX2,Y2,X1,Y1,ALPHA,IERR)
CALL ANGLECX1,Y1,XM,YM,THETA,IERR)
BETA=ABS(ALPHA-THETA+55)
IF(BETA.GE.180.) THEN
  GAMA=360.-BETA
ELSE
  GAMA=BETA
END IF
IF(VF(N,I).LT.0.) THEN
  VVF=AB/(3.*1.852)
  GO TO 116
ELSE
  VVF=VF(N,I)
END IF
PPD=PC(N,I)
IF(PPD.GE.1000.) GO TO 200
IF(VVF.GE.30.) VVF=30.
DELU=0.5*VVF*CCSD(GAMA)
P=ABS(YM-Y1)
A=90.-X1
S=90.-XM
DD=60.*ACOSD(1.-((1.-CCSD(P))*SIND(A)*SIND(B)+(1.-CCSD(A-B))))
DD=AM/1.852
DELP=(1000.+(1000.-PPD)/10.-PPD)/33.86
RPL=(28.+52*TANH(0.0873*(Y1-28.))+12.22*EXP((PPD-1013.2)/33.86)
  +0.2*VVF*1.352+37.22)/1.852
RK=70.-Y1/7.5
UR=(RK*SQR1(DELP)-0.2632*SIND(Y1)*RPL-5.965*SIND(Y1))/(1+
  -0.04386*SIND(Y1))
UR=RK*SQR1(DELP)-0.5*0.5263*RPL
IF(UR.LE.0.) UR=0.01
R=RPL*EXP((PPD-1013.2)/(33.86*2.3))
IF(UR.LT.100.) GO TO 51
R=RPL-((UR-100.)/6.+6.)
GO TO 50
R=RPL
FRU1=0.5263*SIND(Y1)*R/UR
FRU2=0.5263*SIND(Y1)*RPL/UR
IF(DD.EQ.0.) DC=0.0001
SUR=UR*((0.5*FRU1*DD/R)**2.+(1+FRU1)*(R/DD)*EXP(1-R/DD))
**0.5-0.5*FRU1*DD/R)
IF(SUR.LE.0.) SUR=0.1
URA=0.865*SUR
SURA=0.865*SUR
URAA=URA*DELU
SURAA=SURA*DELU
PK1=7.59-41.21*FRU1+160.51*FRU1**2.-219.32*FRU1**3.
PK2=7.59-41.21*FRU2+160.51*FRU2**2.-219.32*FRU2**3.
PK1=PK1.LE.0.) PK1=0.2

```

116

C

C

C51

H-9



15-JUN-1987 04:19

\_DJAI: CCHIEN.CWBJWAVET2.FOR:6

```

IF(PK1.GE.7.59) PK1=7.59
IF(PK2.LE.0.) PK2=0.2
IF(PK2.GE.7.59) PK2=7.59
HR=PK2*SQR(T(RPL*DELP))
HRS=PK2*SQR(T(R*DELP))
RR=DD/R
IF(CRR.LE.10.) GO TO 1000
H13=0.11*HR*RPL/DD*0.5
IF(URAA.LE.0.) GO TO 113
HRA=HR*(1+DELU/URAA)*2.
CALL PERIOD(HRA,URAA,TA,IERR)
IF(IERR.EQ.1) GO TO 113
OTRU=(OD*TA)/(QPL*URAA)
IF(URAA.LE.0.) OTRU=0.2
CP=0.0021*OTRU*2.+0.0012*OTRU+1.21
T13=CP*TA
GO TO 114

```

113  
114

```

T13=10.0
NAME='SWELL'
IF(T13.EQ.0.) GO TO 900
TLAG(N,I,J)=DD/(3.6*0.78*T13)
GO TO 9900
CALL BRET(FRUR1,RR,RH,IERR)
IF(IERR.EQ.1) GO TO 200
IF(QH.GE.1.22) RH=1.2
SHR=HRS*RH

```

1000

```

IF(SURAA.LE.0.) SHR=0.
IF(SURAA.LT.ABS(DELU)) SURAA=4.*ABS(DELU)
SHRA=SHR*(1+DELU/SURAA)*2.
CALL PERIOD(SHRA,SURAA,STA,IERR)
IF(IERR.EQ.1) THEN
  STA=4.0
  IF(SURAA.LE.21.5) SURAA=22.
  CC=8.46/(0.4*SURAA)
  CW=QC+QC*3.73.+CC*5./5.+QC*7./7.
  CA=2.*CW*1.67
  AW=(EXP(COA)-1.)/(EXP(COA)+1.)
  SHRA=(CA*SURAA*SURAA)/40.
ELSE
  SHRA=SHRA

```

```

END IF
H13=SHRA/3.28
T13=4.*SQR(STA)
NAME=' WIND'
TLAG(N,I,J)=0.0
ITYI=ITYCN,I
ITPI=ITM(N,I)
ITDI=IID(N,I)
ITHI=ITH(N,I)
CALL TRIMS(ITYI,ITMI,ITDI,ITHI,IABSTY,IABSTH,I)
KTYCN,I,J)=IABSTH
KTYCN,I,J)=IABSTY
KTHCN,I,J)=IABSTH+TLAG(N,I,J)
HTCN,I,J)=H13
PTCN,I,J)=T13
GO TO 300

```

9900

900.PT:KTYCN,I,J)=IABSTY

15-JUN-1987 04:19

\_DJA1:CHTEN.CWBJWAVET2.FOR:6

```

KTHCN,I,J)=IABSTH
HT(N,I,J)=0.
PT(N,I,J)=0.
300 CONTINUE
200 CONTINUE
100 CONTINUE
RETURN
END
SUBROUTINE PERIOD(X,Y,Z,IERR)
COMMON X,Y,Z,IERR
A=(40.*X)/Y**2.
IF(A.GE.1.) GO TO 10.
B=ALOG((1+A)/(1-A))
C=(0.5*B)**0.6
D=0.*TANH(C)*Y
Z=(4./5.)*0.25*D
IERR=0
GO TO 1
IERR=1
RETURN
END
SUBROUTINE BRET(FRUR,RR,RATE,IERR)
DIMENSION A(10),C(10,10),V(10)
CHARACTER*2 PA
IERR=0
A(1)=0.
A(2)=0.02
A(3)=0.04
A(4)=0.06
A(5)=0.10
A(6)=0.15
A(7)=0.20
A(8)=0.30
A(9)=0.50
C(1,1)=0.10017835E-5
C(1,2)=-0.61861162E-4
C(1,3)=0.14723198E-2
C(1,4)=-0.1790538E-1
C(1,5)=0.12099124
C(1,6)=-0.45196415
C(1,7)=0.7997339
C(1,8)=0.54218079
C(2,1)=-0.85238E-6
C(2,2)=0.17119E-4
C(2,3)=0.9522E-4
C(2,4)=-0.521E-2
C(2,5)=0.54727E-1
C(2,6)=-0.259325
C(2,7)=0.5031576
C(2,8)=0.705566
C(3,1)=0.0
C(3,2)=-0.81968951E-5
C(3,3)=0.373249E-3
C(3,4)=-0.65767033E-2
C(3,5)=0.575878E-1
C(3,6)=-0.26153058
C(3,7)=0.48609795
C(3,8)=0.72522351

```



```

C(4,1)=-0.610529E-5
C(4,2)=0.22E-3
C(4,3)=-0.3072E-2
C(4,4)=0.2041E-1
C(4,5)=-0.59381E-1
C(4,6)=0.173E-1
C(4,7)=0.1285E23
C(4,8)=0.89655E46
C(5,1)=0.0
C(5,2)=-0.145E-4
C(5,3)=0.567342E-3
C(5,4)=-0.889732E-2
C(5,5)=0.713E-1
C(5,6)=-0.29734355
C(5,7)=0.45821415
C(5,8)=0.77636381
C(6,1)=-0.13371897E-4
C(6,2)=0.52797074E-3
C(6,3)=-0.8410413E-2
C(6,4)=0.68857376E-1
C(6,5)=-0.30413751
C(6,6)=0.6923571
C(6,7)=-0.8973324
C(6,8)=1.4709649
C(7,1)=0.0
C(7,2)=-0.13745E-4
C(7,3)=0.5212115E-3
C(7,4)=-.7994E-2
C(7,5)=0.6265148E-1
C(7,6)=-0.246345
C(7,7)=0.2671735
C(7,8)=0.92671
C(8,1)=0.0
C(8,2)=-0.23091255E-4
C(8,3)=0.92845633E-3
C(8,4)=-0.14887704E-1
C(8,5)=0.11305687
C(8,6)=-0.46714977
C(8,7)=0.60754091
C(8,8)=0.74695602
C(9,1)=0.74204823E-5
C(9,2)=-0.31812369E-3
C(9,3)=0.56303258E-2
C(9,4)=-0.52851118E-1
C(9,5)=0.27785340
C(9,6)=-0.76195305
C(9,7)=0.68421671
C(9,8)=0.84775850
IF(CR.LI.1) GO TO 1000
RE=RR
FA=FRUR
DO 100 I=1,9
V(I)=C(I,1)*RE**7+C(I,2)*RE**6+C(I,3)*RE**5+C(I,4)*RE**4
+C(I,5)*RE**3+C(I,6)*RE**2+C(I,7)*RE+C(I,8)
DO 200 I=1,9
IF((FA-A(I)).GT.0.) GO TO 200
K=I

```



15-JUN-1987 04:19

\_OJAI:[CHSEN.CWB]MAVET2.FOR:6

```

200 CONTINUE
   HR=V(C9)
   GO TO 500
400 IF(K.EQ.1)GO TO 600
   HR=((CFA-A(K-1))/(ACK)-A(K-1))*(V(K)-V(K-1))+V(K-1)
   GO TO 500
600 HR=V(C1)
500 RATE=HR
   GO TO 900
1000 RATE=1.
   RETURN
900
END
SUBROUTINE ANGLE(X1,Y1,X2,Y2,ANG,IERR)
  IERR=0
  AY=Y1-Y2
  AX=X1-X2
  IF(AX.EQ.0.) GC TO 20
  ANG=ATAN2(AY/AX)
  IF(AX.GT.0.) THEN
    ANG=ANG
  ELSE
    ANG=ANG+180.
  END IF
  GO TO 200
  IF(AY.EQ.0.) GC TO 50
  IF(AY.GT.0.) THEN
    ANG=90.
  ELSE
    ANG=270.
  END IF
  GO TO 200
  IERR=1
  RETURN
END
SUBROUTINE SUBT(I,K,M,TLAT,TLON,PO,VF,R,WS,WLON,WLAT)
  DIMENSION TLAT(4,160),TLON(4,160),PO(4,160),VF(4,160),R(4,160)
  DIMENSION WS(150,1200),WLON(150),WLAT(150)
  IF(R(I,K).GT.0.) GC TO 5
  RPL=(28.52*TANH(0.0873*(TLAT(I,K)-28.)))*12.22*EXP((PO(I,K)-1013.2)
  -/33.86)+0.2*VF(I,J)*1.852*37.22)/1.852
  GO TO 10
  RPL=R(I,K)
  XA=TLON(I,K)
  YA=TLAT(I,K)
  DO 100 J=1,150
    XM=WLON(J)
    YM=WLAT(J)
    CALL OIS(XA,Y4,XM,YM,RO)
    IF(RO.GE.(RPL*9.5)) GO TO 100
    WS(J,M)=0.
  CONTINUE
  RETURN
END
SUBROUTINE SHEL(T(XI,YI,XM,YM,XX,YU,YD,YY,XU,XD,XL,YL,JEER,
  I,II,III)
  DIMENSION XL(500),YL(500),XX(200),YU(200),YD(200),YD(200)
  DIMENSION YX(200),XU(200),XD(200),XD(200)

```



```

MM(10)=274
MM(11)=305
MM(12)=335
IF(ICODE.GT.0) GO TO 60
GO TO 20
MM(1)=0
MM(2)=31
MM(3)=59
MM(4)=90
MM(5)=120
MM(6)=151
MM(7)=181
MM(8)=212
MM(9)=243
MM(10)=273
MM(11)=304
MM(12)=334
IF(ICODE.GT.0) GO TO 60
GO TO 20
IABSY=IY
IABSH=MM(IM)*24+(IO-I)*24+IH
GO TO 100
MM=(MM(12)+31)*24
IF(IABSH.GT.MMM) GO TO 40
GO TO 25
IABSH=IABSH-MMM
WRITE(5,70)IABSH,MM
FORMAT(5X,'IABSH=',I5,'      MMM=',I5)
IY=IABSY+1
IM=1
IK=IABSH/24
IJ=IK*24
IH=IABSH-IJ
IO=IK+1
GO TO 100
IK=IABSH/24
IJ=IK*24
IH=IABSH-IJ
OO 30 I=1,12
IF(IK.GE.MP(I)) GO TO 35
IM=I-1
GO TO 45
35 IF(I.EQ.12) IM=12
30 CONTINUE
45 IO=IK-MP(IM)+1
IY=IABSY
RETURN
END
SUBROUTINE ANGCKA,YA,XM,YM,CO,IEER)
DY=YA-YM
DX=XA-XM
IEER=0
IF(DX.EQ.0.AND.DY.EQ.0.) GO TO 9999
IF(DX.EQ.0.AND.DY.GT.0.) GO TO 505
IF(DX.EQ.0.AND.DY.LT.0.) GO TO 510
GO TO 550
505 CO=0.
GO TO 600

```

```

510 CO=180.
GO TO 600
550 CO=ATAND(OY/OK)
IF(COX.GT.0.AND.OY.GT.0.) GO TO 525
IF(COX.LT.0.) GO TO 530
IF(COX.GT.0.AND.OY.LT.0.) GO TO 525
GO TO 600
525 CO=90-CD
GO TO 600
530 CO=270.-CD
GO TO 600
9999 IEER=1
500 RETURN
END
SUBROUTINE MPTLV(LK,KTY,KKTH,MT,TLAG)
C
C THIS PROGRAM IS MCOIFY THE WAVE HEIGHT AND PERIOD.
C IT'S CONSIDER THE SUPERPOSITION , OVERLAPPED , . . . ETC
C WHEN TIME LAG IS CHANGE.

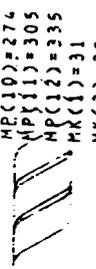
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```

DIMENSION MP(12),MK(12),ST(2),AT(2),LK(4)
DIMENSION IM(120),IO(120),IH(120),IY(120),ITL(120)
DIMENSION ITT(120),HE(120),AHE(120),AAHE(120)
DIMENSION KTY(4,120,100),KKTH(4,120,100),HT(4,120,100)
DIMENSION TLAG(4,120,100)
INTEGER AIM(120),AIO(120),AHC(120),FLAG(120),FLAG1
DO 4000 M=1,4
KA=LK(M)
DO 5000 J=1,89
DO 6000 N=2,KA
IABSYC=KTY(M,N,J)
IABSHC=KKTH(M,N,J)
CALL TRTIMECIY,IMH,IOO,IHM,IABSYC,IABSHC,-1)
ITL(N)=TLAG(M,N,J)
HE(N)=HT(M,N,J)
IM(N)=IMH
IO(N)=IOO
IH(N)=IHM
IY(N)=IY
CONTINUE
RY=1911+IYY
FY=RY/4.
KY=RY/4.
IF((FY-KY).GT.0.001) GO TO 50
MP(1)=0
MP(2)=31
MP(3)=60
MP(4)=91
MP(5)=121
MP(6)=152
MP(7)=182
MP(8)=213
MP(9)=244
MP(10)=274
MP(11)=305
MP(12)=335
MK(1)=31
MK(2)=29

```

5000

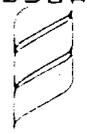


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MK(3)=31
MK(4)=30
MK(5)=31
MK(6)=30
MK(7)=31
MK(8)=31
MK(9)=30
MK(10)=31
MK(11)=30
MK(12)=31
GO TO 20
MP(1)=0
MP(2)=31
MP(3)=59
MP(4)=90
MP(5)=120
MP(6)=151
MP(7)=181
MP(8)=212
MP(9)=243
MP(10)=273
MP(11)=304
MP(12)=334
MK(1)=31
MK(2)=28
MK(3)=31
MK(4)=30
MK(5)=31
MK(6)=30
MK(7)=31
MK(8)=31
MK(9)=30
MK(10)=31
MK(11)=30
MK(12)=31
DO 200 NA=1,KA
  NNH=IH(HA)+ITL(NA)
  NUD=NNH/24
  AIH(NA)=NNH-NUD*24
  NND=ID(N4)+NUD
  IFCNND.GT.*K(IH(NA))) THEN
    AIM(NA)=IM(NA)+1
    AID(NA)=NND-MK(IM(NA))
  ELSE
    AIM(NA)=IM(NA)
    AID(NA)=NND
  END IF
200 CONTINUE
DO 220 NB=1,KA
  ITT(NB)=MP(AIM(NB))*24+(AID(NB)-1)*24+AIH(NB)
  II=1
  IF(II.GT.KA) GO TO 99
  WRITE(5,*)II
  LTT=ITT(II)
  U=b
  DO 600 JA=II+1,KA
    IFC(IIT(JA).LE.LTT) THEN
      LTT=ITT(JA)

```



```

        L=JA
        ELSE
            GO TO 600
    END IF
    CONTINUE
    IF(L.EQ.0) THEN
        AHE(II)=ME(II)
    ELSE
        SUMH=0.
        DO 620 IP=II,L
            SUMH = SUMH + ME(IP) * ME(IP)
            HH=SQR(SUMH)
        DD 640 IJ=II,L
            AHE(IJ)=HH
            IYL(IJ)=-1
        GO TO 500
    END IF
    II=II+1
    GO TO 88
    II=L+1
    GO TO 88
    FLAG(1)=100
    DO 1000 LP=2,K
        IF(IYL(LP).EQ.-1) THEN
            FLAG(LP)=100
            GO TO 1000
        ELSE
            IF(IYL(LP-1).EQ.-1) THEN
                FLAG(LP)=100
                GO TO 1000
            ELSE
                IF(IYL(LP)-IYL(LP-1)) 1005,1010,1015
                    GO TO 1000
            END IF
        END IF
    END IF
    CONTINUE
    DO 1500 JI=1,K
        AAME(JI)=AME(JI)
        LL=2
        IF(LL.GT.K) GO TO 3000
        IF(FLAG(LL).EQ.1) THEN
            FLAGI=1
            GO TO 2400
        ELSE
            IF(FLAG(LL).EQ.-1) THEN
                FLAGI=-1
                GO TO 2400
            ELSE
                GO TO 2000
            END IF
        END IF
    DD 2450 I=LL,K
        IF(FLAG(I).EQ.FLAGI) GO TO 2450

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15-JUN-1987 04:19

2400 00 2450 I=LL,KA  
IF(FLAG(I).EQ.FLAGI) GO TO 2450

-DJAI: CCHIEN.CWB3WAVET2.FOR:6

```

II=I-1
GO TO 2460
CONTINUE
II=KA
2460 ST(1)=MP(IM(LL-1))*24+(ID(LL-1)-1)*24+IH(LL-1)
ST(2)=MP(IM(II))*24+(ID(II)-1)*24+IH(II)
AT(1)=MP(AIM(LL-1))*24+(AID(LL-1)-1)*24+AIM(LL-1)
AT(2)=MP(AIM(II))*24+(AID(II)-1)*24+AIM(II)
TONEY=((ST(2)-ST(1))/(AT(2)-AT(1)))*0.5
DO 2900 NH=LL,II
AAHE(NH)=AHE(NH)*TONEY
LL=II+1
GO TO 2800
2000 LL=LL+1
GO TO 2800
3000 DO 3000 NG=1,KA
300 HT(N,J)=AAHE(NC)
5000 CONTINUE
4000 CONTINUE
RETURN
END
SUBROUTINE DIS(XA,YA,XB,YB,DDD)
XX1=XA*111.324*CODS(YA*3.14159/180.)
YY1=YA*111.324
XX2=XB*111.324*CODS(YB*3.14159/180.)
YY2=YB*111.324
DDD=SQRT((XX1-XX2)**2.+(YY1-YY2)**2.)
RETURN
END
SUBROUTINE EAREA(RR,RLU,RL,DA,CD)
DIMENSION R(2),A(2)
AL=111.12
R(1)=RL
R(2)=RLU
IF(CD.GT. 90.AND.CD.LE.180) GO TO 101
IF(CD.GT.180.AND.CD.LE.270) GO TO 102
IF(CD.GT.270.AND.CD.LE.360) GO TO 103
GO TO 100
101 CD=180.-CD
GO TO 100
102 CD=CD-180.
GO TO 100
103 CD=360.-CD
GO TO 100
SCL=55.6*(SIND(CD)+COSD(CD))
SSCL=55.6*ABS(COSD(CD)-SIND(CD))
DO 50. K=1,2
DR=ABS(R(K)-RR)
IF(CD.LT.0.05.DR.(90.-CD).LT.0.05) GO TO 500
IF(DR.GE. SCL) GO TO 52
IF(DR.GE. SSCL) GO TO 53
AK)=(SSCL-DR)*AL)/COSD(CD)+AL*AL*TAND(CD)/2.
GO TO 50
53 AK)=(SSCL-DR)/(AL*SIND(CD))**2.*(AL*AL*TAND(CD))/2.
GO TO 50
52 AK)=0.
GO TO 50
500 IF(CD.LT.55.6) GO TO 501
IF(CD.LT.55.6) GO TO 501
IF(CD.LT.55.6) GO TO 501

```

53  
52  
500

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\_OJAI:ECMIEN.CWB3WAVET2.FOR:6

```
501 GO TO 50
50  A(K)=(55.6-OR)*AL
    CONTINUE
    IF(R(1).LE.RR.AND.R(2).LE.RR) GO TO 201
    IF(R(1).LE.RR.AND.R(2).GE.RR) GO TO 202
    TA=A(1)-A(2)
    GO TO 200
    201 TA=A(2)-A(1)
    GO TO 200
    202 TA=AL*AL-A(1)-A(2)
    200 DA=(TAN*DA)/(AL*AL)
    RETURN
    END
```

11/10/87

## 附 錄 II 可用於個人電腦之波浪預報系統程式

洪 憲 忠

本附錄乃針對 IBM 個人電腦 (IBM PC/XT) 而設計之本計劃程式，由於使用標準的 FORTRAN 77 電腦語言，故此程式可輕易地轉移至 VAX-11 780 電腦上使用。

爲了使程式可在 IBM PC/XT 上使用，因此，將波浪預報系統之程式進行分割再整合。其各程式之功能概述如下：

1. MONSOON.FOR:

求季風風場下波浪點之波高及週期。

2. TWINDW.FOR:

求颱風 10 R 範圍內波浪點之波高及週期。

3. TSWELL.FOR:

求由於湧浪造成之波浪點波高及週期。

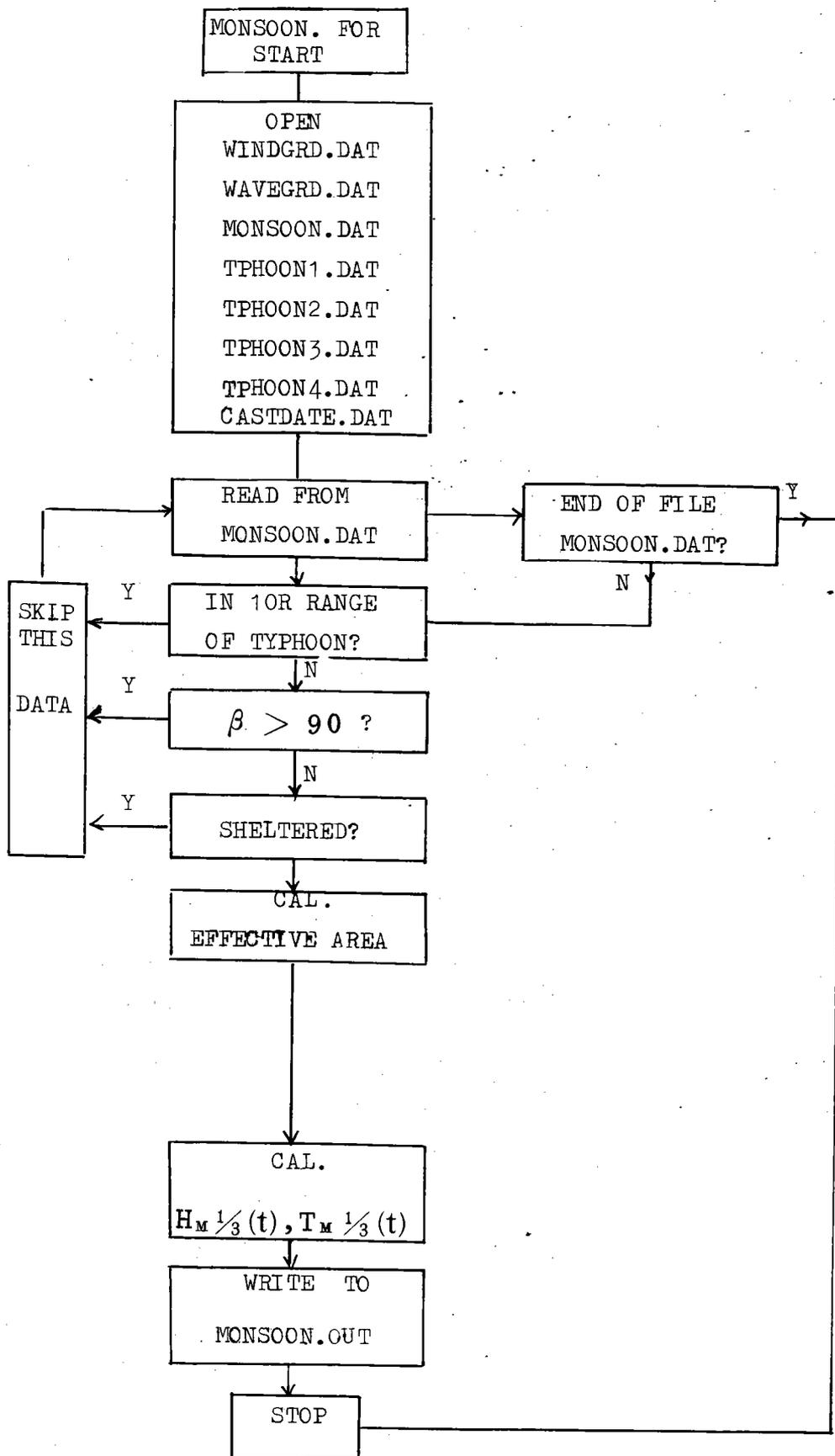
4. SUMCWB.FOR:

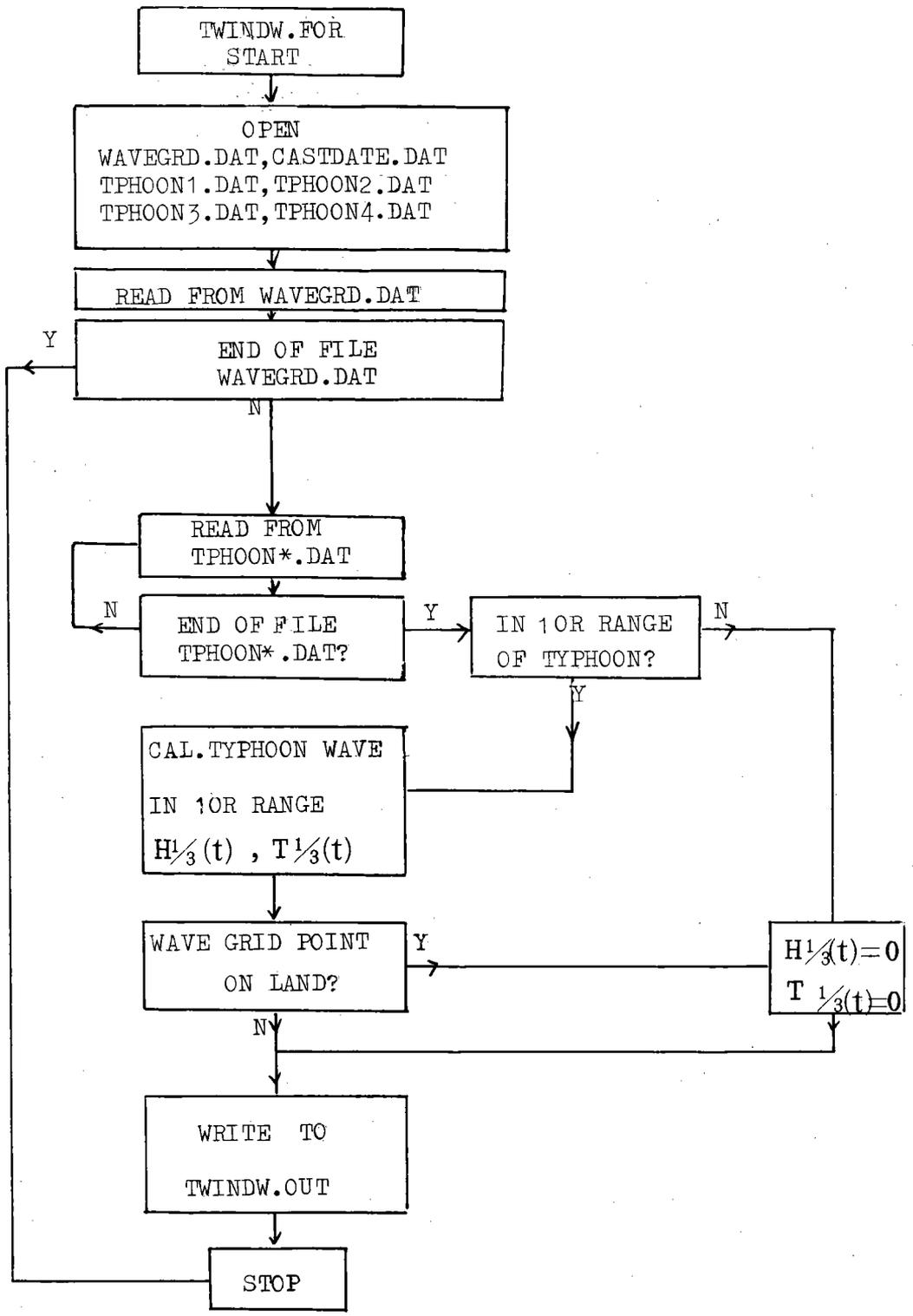
將季風、颱風風浪、湧浪三者整合而得三者共同作用下波浪點之波高及週期。

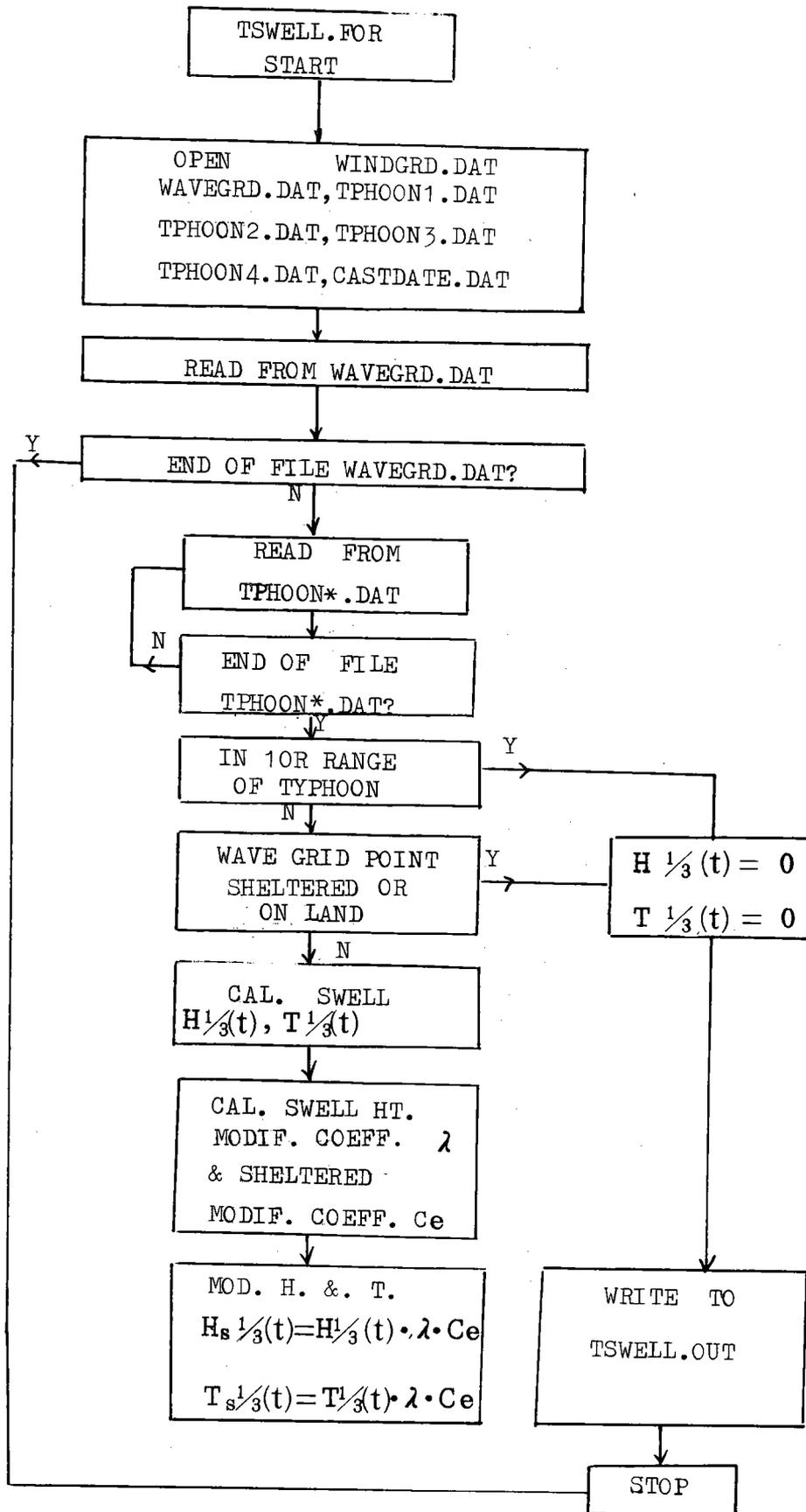
5. CWBLIB.FOR:

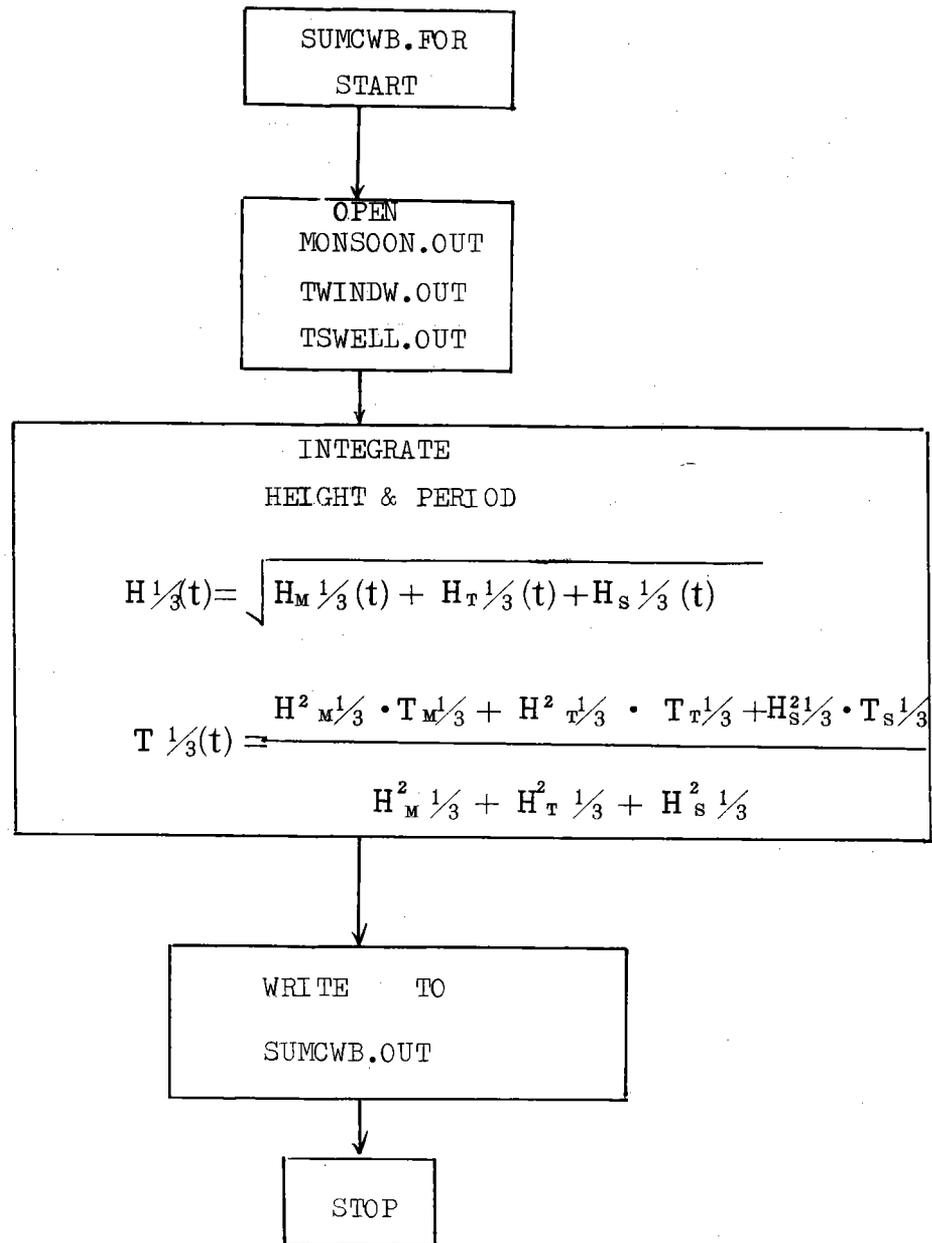
提供前述各程式所須之副程式程式庫。

平常，系統運作，須用到之主程式有 MONSOON.FOR、TWINDW.FOR、TSWELL.FOR 及 SUMCWB.FOR 等四者，其簡要流程圖各如下述：









各程式列印如后：



```

C      CCY2: CARTESIAN Y-COORDINATE OF WIND GRID POINT.
      CALL LONLTCXA, YA, LON1(I1), YA, CCX1(I1))
      CALL LONLTCXA, YA, XA, LAT1(I1), CCY1(I1))
      NG1=NG1+1
      GO TO 33
34      NG1=NG1-1
      REWIND 1
      IF(NG1 .NE. NCMAX1) THEN
        WRITE(*,*) 'PLS CHECK ALLOWABLE WIND GRID NO DIMENSION'
      END IF

      NG2=1
      REWIND 8
      READ(8,*)
      READ(8,*, END=37) I2, LON2(I2), LAT2(I2)
      READ(8,*, END=37) I2, LON2(I2), LAT2(I2), CUSI(I2)
      CHANGE (LONGITUDE, LATITUDE) INTO CARTESIAN COORDINATE.
      CCX2: CARTESIAN X-COORDINATE OF WAVE GRID POINT.
      CCY2: CARTESIAN Y-COORDINATE OF WAVE GRID POINT.
      CALL LONLTCXA, YA, LON2(I2), YA, CCX2(I2))
      CALL LONLTCXA, YA, XA, LAT2(I2), CCY2(I2))
      NG2=NG2+1
      GO TO 36
37      NG2=NG2-1
      REWIND 8
      IF(NG2 .GT. NCMAX2) THEN
        WRITE(*,*) 'PLS CHECK ALLOWABLE WAVE GRID NO DIMENSION'
      END IF

      DO 343 I2=1,NG2
        READ(13,*)
        READ(13,*) IO, CUSI(I2)
        IF(I2 .NE. IO) THEN
          WRITE(*,*) 'PLS CHECK FILE CUSI.DAT.'
        END IF
343      CONTINUE

      IF(NT .GT. NCMAX ) THEN
        WRITE(*,*) 'TOTAL TIME NO IS OVER ALLOWABLE.'
      END IF

      REWIND 11
      READ(11,*)
      READ(11,*) C3, C4
      REWIND 11

      REWIND 3
      READ(3,*)
      NW=1
      READ(3,*, END=28) NY3(NW), NMCN3(NW), NOD3(NW), NHR3(NW)
      GO TO 26
28      NW=NW+1
      REWIND 12
      DO 80 I=1,NG2
      DO 82 J=1,NG1
        CALL LONLTC(LON1(J), LAT1(J), LON2(I), LAT2(I), DDIST(J))

```

```

82 CONTINUE
C THE JTH FIELD DATA OF THE ITH RECORD IN FILE 12 REPRESENTS
C THE DISTANCE OF ITH WAVE GRID POINT TO JTH WIND GRID POINT.
WRITE(12) (OOIST(J),J=1,NG1)
80 CONTINUE
REWIND 12
C CHANGE H13(CM) INTO H13(M).
C CHANGE T13(10 SEC) INTO T13(SEC).
H13(CM)=H13(NM)/100.
T13(CM)=T13(NM)/10.
C NM: FORECASTED WAVE TIME NO.
DO 1000 I1=1,NM
REWIND 12
C WRITE(10,123) I1
WRITE(10,132)
C WRITE(10,134) NYY3(I1),NMON3(I1),NDD3(I1),NHR3(I1)
WRITE(10,*)
WRITE(10,136)
C WRITE(*,*)
WRITE(*,*) ' FORECAST WAVE NO=',I1
WRITE(*,132)
WRITE(*,134) NYY3(I1),NMON3(I1),NDD3(I1),NHR3(I1)
WRITE(*,*)
WRITE(*,136)
C
C 123 FORMAT('1','FORECAST WAVE NO=',I2)
132 FORMAT(1X,'Y',2X,'NM',1Y,'DD',1Y,'HR')
134 FORMAT(1X,I4,3I3)
136 FORMAT(3X,'PT.',5Y,'LON',8X,'LAT',7X,'H13(CM)',
1 4X,'T13(S)')
C DO 1010 K=1,NG2
C WRITE(*,*) 'WAVE GRID POINT=',K
CXM=CCX2(K)
CYM=CCY2(K)
READ(12) (OOIST(JJ),JJ=1,NG1)
SH=0.
MAXF=0
SUA=0
SA=0
112 READ(2,*,END=114) NYY,NMON,NDD,NHR
READ (2,*)
KYY3=NY3(I1)
KMCN3=NMON3(I1)
KDD3=NDD3(I1)
KHF3=NHR3(I1)
CALL TINDUR(NYY,NMON,NDD,NHR,KYY3,KMCN3,KDD3,KHF3,TO)
IF(TD.LT.0) THEN
GO TO 114
END IF
DO 120 J=1,NG1
WRITE(*,*) 'WIND GRID NO=',J
DO 200 IP=1,NPHOON
IF(IP.EQ.1) READ(4,*,END=200)
IF(IP.EQ.2) READ(5,*,END=200)

```

II - 8

2772

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IF(IP .EQ. 3) READ(6,*,END=200)
IF(IP .EQ. 4) READ(7,*,END=200)
IF(IP .EQ. 1) THEN
  READ(4,*,END=200) TTY,TMM,TDD,THR,TLON,TLAT,
  PO,VF,R10,R7,TMANG
ELSE IF(IP .EQ. 2) THEN
  READ(5,*,END=200) TTY,TMM,TDD,THR,TLON,TLAT,
  PO,VF,R10,R7,TMANG
ELSE IF(IP .EQ. 3) THEN
  READ(6,*,END=200) TTY,TMM,TDD,THR,TLON,TLAT,
  PO,VF,R10,R7,TMANG
ELSE IF(IP .EQ. 4) THEN
  READ(7,*,END=200) TTY,TMM,TDD,THR,TLON,TLAT,
  PO,VF,R10,R7,TMANG
END IF
CALL LONLTD(TLON,TLAT,LONI(J),LATI(J),DISTI)
WRITE(*,*) 'DISTI=',DISTI
WRITE(*,*) 'R7=',R7
WRITE(*,*) 'NYY,TTY=',NYY,TTY
WRITE(*,*) 'NMON,TMM=',NMON,TMM
WRITE(*,*) 'NDD,TDD=',NDD,TDD
WRITE(*,*) 'NHR,THR=',NHR,THR
IF(NYY.EQ.TTY .AND. NMON.EQ.TMM .AND. NDD.EQ.TDD
  .AND. NHR.EQ.THR .AND. DISTI .LE. R7) THEN
  READ(2,*) NPT,RNUL,RNUU,WU,WD
  GO TO 120
END IF
GO TO 220
CONTINUE
REWIND 4
REWIND 5
REWIND 6
REWIND 7
LATJ=INT(LATI(J))
WRITE(*,*) 'LATI(J)=' ,LATI(J)
WRITE(*,*) 'LATJ=' ,LATJ
WRITE(*,*) 'LATJ,AREA(LATJ)=' ,LATJ,AREA(LATJ)
WU: WIND SPEED (M/S).
WD: WIND DIRECTION (DEGREE, FROM +X AXIS).
READ(2,*) NPT,RNUL,RNUU,WU,WD
WRITE(*,*) 'LONI(J),LATI(J)=' ,LONI(J),LATI(J)
WRITE(*,*) 'NPT,WU=' ,NPT,WU,WD
WRITE(*,*) 'DIST=' ,ODIST(J)
WRITE(*,*) 'WU=' ,WU
WRITE(*,*) 'TD=' ,TD
WRITE(*,*) 'DIST-WU*3600.*TD/2./1000.= ' ,
DIST(J)-WU*3600.*TD/2./1000.
1.8=3600/2./1000.
WRITE(*,*) 'THE DISTANCE DIFFERENCE =' ,DI
CALL ANGLE(CXM,CYM,CCXI(J),CCYI(J),ANG)
AI: THE ANGLE BETWEEN WIND DIRECTION AND DIRECTION
  FROM WIND GRID POINT TO MEASURING STATION.
AI=ABS(CANG-WD)
WRITE(*,*) 'THE BETA ANGLE =' ,AI
IF(AI.GT.90) GO TO 120
CALL SHELTC(XM,CYM,CCXI(J),CCYI(J),NCODE,MAXITR)
WRITE(*,*) 'NCODE=' ,NCODE
IF(NCODE .EQ. 0) THEN

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\_OJAI:CHORNGJMONSOON.FOR:84

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C * WRITE(*,*) 'WIND GRID NO=' , J
C WRITE(*,*) 'CCX2,CCY2,CCX1,CCY1',CYM,CYM,CCX1(J),CCY1(J)
C END IF
C IF(CHCODE .GE. 1) GO TO 120
C IF(DDIST(J) .GT. MAXF) MAXF=DDIST(J)
C IF(LON1(J).EQ.LON2(K) .AND. LAT1(J).EQ.LAT2(K)) GO TO 120
C
C CAL. EFFECTIVE AREA.
C
C RI(1)=WU*TD*1.8
C TD+3.: MONSOON FILE'S CATAI'S TIME LAG=3 HR.
C RI(2)=WU*(TD+3.)*1.8
C IF(ANG .LE. 180.) THEN
C THITA: DEGREES
C THITA=ABS(ANG-90.)
C ELSE
C THITA=ABS(270.-ANG)
C END IF
C THITA2: RADIAN
C THITA2=0.0174533*THITA
C COS1=COS(THITA2)
C SIN1=SIN(THITA2)
C TAN1=TAN(THITA2)
C COS2=COS1+SIN1
C COS3=ABS(COS1-SIN1)
C GL=SQRT(AREA(LATJ))
C GL2=0.5*GL
C DD 62 IZ=1,2
C RDD(IZ)=ABS(RI(IZ))-DDIST(J))
C IF(THITA.EQ.0 .OR. THITA.EQ.90.) THEN
C IF(RDD(IZ).GE.GL2) THEN
C AI(IZ)=0.
C ELSE
C AI(IZ)=(GL2-RDD(IZ))*GL
C END IF
C ELSE IF(RDD(IZ).GE.GL2*CCS2) THEN
C AI(IZ)=0.
C ELSE IF(RDD(IZ).LT.GL2*CCS2 .AND. RDD(IZ).GE.GL2*CCS3)
C THEN
C AI(IZ)=(GL**2)/2.*TAN1*((GL2*CCS2-RDD(IZ))/
C (GL*SIN1))**2
C ELSE
C AI(IZ)=(GL2*CCS3-RDD(IZ))*GL/COS1+(GL**2)/
C 2.*TAN1
C END IF
C CONTINUE
C IF(RI(1).LE.DDIST(J) .AND. RI(2).LE.DDIST(J)) THEN
C EAREA=AI(2)-AI(1)
C ELSE IF(RI(1).LT.DDIST(J) .AND. RI(2).GT.DDIST(J)) THEN
C EAREA=GL**2-AI(2)-AI(1)
C ELSE IF(RI(1).GT.DDIST(J) .AND. RI(2).GT.DDIST(J)) THEN
C EAREA=AI(1)-AI(2)
C END IF
C
C SUA=SUA+WU*EAREA
C WRITE(*,*) 'SUA=' , SUA
C SA=SA+EAREA
C WRITE(*,*) 'SA=' , SA

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CHORNGJMONSOON

```

WUZ=WU**2
C 0.00008=0.08/1000.
C 0.0174533=3.14159/180.
SH=SH+WUZ*(COS(A1*0.0174533)**2)*
EXP(-0.08*DDIST(J)/WUZ)*EAREA/DDIST(J)*1000.
120 *
CONTINUE
100 GO TO 112
C UBAR: UNIT (M/SEC).
C MAXF: (KM).
C WRITE(*,*) 'SUA=',SUA
C WRITE(*,*) 'SA=',SA
114 IFCSA -EQ. 0 -OR. SUA -EQ. 0 -OR. MAXF -EQ. 0 GO TO 999
UBAR=SUA/SA
C 0.64114=2**3.14159/9.8
UBAR2=UBAR**2
C T13:(SEC)
C T13(K)=0.64114*C3*((9800.*MAXF/UBAR2)**C4)*UBAR
C 0.8163265=8/9.8
C H13:(M)
C H13(K)=(0.8163265*CUSI(K)*SH/T13(K))*0.5
999 REWIND 2
WRITE(10,138) K,LON2(K),LAT2(K),100.*H13(K),T13(K)
WRITE(*,138) K,LON2(K),LAT2(K),100.*H13(K),T13(K)
FORMAT(IX,I4,4(IX,F10.3))
138 CONTINUE
1010 CONTINUE
130 STOP
FORMAT('DATE:',4(C2X,I4))
END

```

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\_DJAI:[HORHG]TWINDM.FOR:16

C PROGRAM TWINCH.FOR (ONLY CONSIDER WIND WAVE OF TYPHOON).

C NG2MAX: ALLOWABLE MAX. GRID NO OF WAVE FIELD.

C NPHOON: ALLOWABLE MAX. NO OF TYPHOON.

C PARAMETER (NG2MAX=200, NPHOON=4)

REAL LON2(NG2MAX),LAT2(NG2MAX),LON22,LAT22

INTEGER TTY,TMM,TD0,THR,CYY,CMM,CDD,CHR

DIMENSION CX2(NG2MAX),CY2(NG2MAX)

OPEN(UNIT=1,FILE='WAVEGRO.DAT',STATUS='OLD')

OPEN(UNIT=2,FILE='TYPHOON1.DAT',STATUS='OLD')

OPEN(UNIT=3,FILE='TYPHOON2.CAT',STATUS='OLD')

OPEN(UNIT=4,FILE='TYPHOON3.CAT',STATUS='OLD')

OPEN(UNIT=5,FILE='TYPHOON4.DAT',STATUS='OLD')

OPEN(UNIT=6,FILE='TWINDM.OUT',STATUS='NEW')

OPEN(UNIT=10,FILE='CASTDATE.DAT',STATUS='OLD')

NG2=1

REWIND 1

READ(1,\*)

36 READ(1,\*,END=37) I2,LON2(I2),LAT2(I2)

NG2=NG2+1

GO TO 36

37 NG2=NG2-1

REWIND 1

C NDATE: TIME NO FOR FORECASTING WAVE.

READ(10,\*)

NDATE=1

33 READ(10,\*,END=34) CYY,CMM,CDD,CHR

NDATE=NDATE+1

GO TO 33

34 NDATE=NDATE-1

REWIND 10

READ(10,\*)

READ(1,\*)

DO 128 JG=1,NG2

READ(1,\*) J,LON2(J),LAT2(J)

CONTINUE

128 XA=100.

YA=5.

LON22=121.

LAT22=23.

SHH=0.

STT=0.

DO 988 JJ=1,NDATE

READ(10,\*) CYY,CMM,CDD,CHR

WRITE(6,132)

WRITE(6,134) CYY,CMM,CDD,CHR

WRITE(6,135)

WRITE(\*,\*)

WRITE(\*,\*)

WRITE(\*,\*) 'FORECAST WAVE NO=',JJ

WRITE(\*,\*)

WRITE(\*,132)

WRITE(\*,134) CYY,CMM,CDD,CHR

WRITE(\*,\*)

WRITE(\*,136)

FORMAT('1',FORECAST WAVE NO=',I2)

123 FORMAT(1X,'YY',2X,'MM',1X,'DD',1X,'HR')

132 FORMAT(1X,'I4',14,3I3)

134



```

C      WAVE PERIOD: (S)
C      RMAX=R7/10.*0.53936
C      WRITE(*,*) 'RMAX=',RMAX
C      UR=RK*(CP**0.5)-0.5*RF*RMAX
C      WRITE(*,*) 'UR=',UR
C      URS=0.865*UR
C      WRITE(*,*) 'URS=',URS
C      CHANGE (LONITUDE,LATITUDE) INTO CARTESIAN COORDINATE.
C      (LON,LAT.) OF CARTESIAN COORDINATE ORIGIN (XA,YA) TO BE (100,5).
C      CCX2: CARTESIAN X-COORDINATE OF WIND GRID POINT.
C      CCY2: CARTESIAN Y-COORDINATE OF WIND GRID POINT.
C      CTLON: CARTESIAN X-COORDINATE OF TYPHOON CENTER.
C      CTLAT: CARTESIAN Y-COORDINATE OF TYPHOON CENTER.
C      CALL LONLTC(XA,YA,TLON,YA,CTLON)
C      CALL LONLTD(XA,YA,XA,TLAT,CTLAT)
C      CALL ANGLECCX2(J),CCY2(J),CTLON,CTLAT,TANG)
C      CALL HTI(TANG,THANG,VF,URS,RF,RMAX,UR,CP,DO,
C              FRUR,SRR,HRM,HSRM)
C      CALL PERIOD(CFRUR,ISRR,UR,DU,HSRM,TSRM)
C      GO TO 222
C      END IF
C      GO TO 220
C      SHH=SHH+HSRM**2
C      STT=STT+TSRM*(HSRM**2)
C      WRITE(*,*) 'SHH=',SHH
C      WRITE(*,*) 'STT=',STT
C      CONTINUE
C      IF(SHH .EQ. 0.) THEN
C          T13=0.
C          H13=0.
C          GO TO 111
C      END IF
C      WRITE(*,*) 'AFTER 200,SHH=',SHH
C      T13=STT/SHH
C      H13=SHH**0.5
C      WRITE(6,138) J,LON2(J),LAT2(J),30.48*H13,T13
C      WRITE(6,138) J,LON2(J),LAT2(J),30.48*H13,T13
C      FORMAT(1X,I4,4(1X,F10.3))
C      SHH=0.
C      STT=0.
C      REWIND 2
C      REWIND 3
C      REWIND 4
C      REWIND 5
C      CONTINUE
C      CONTINUE
C      STOP
C      END

```

```

C-----
C      SUBROUTINE FK(FI,RF,RK)
C      FI: INPUT LATITUDE OF TYPHOON CENTER.
C      FFI: LATITUDE ARRAY OF TYPHOON CENTER.
C      FIF: F IN CHART.
C      FIK: K IN CHART.
C      PARAMETER (NI=9)
C      DIMENSION FFI(NI),FIF(NI),FIK(NI)
C      DATA FFI/20.,22.5,25.,27.5,30.,32.5,35.,37.5,40.0/
C      DATA FIF/0.,18.,0.20,0.22,0.24,0.25,0.28,0.30,0.32,0.34/

```

```

DATA FIK/67.,67.,67.,66.,66.,66.,66.,66.,65.,64./
CALL SPLING(NI,FFI,FI,RF)
CALL SPLING(NI,FFI,FI,RF)
RETURN
END

```

```

C-----
C SUBROUTINE KPRAN(FRUF,RK1)
C FRUF: FR/UR IN CHART
C PARAMETER (NI=51)
C DIMENSION FRU(NI),AKP1(NI)
DATA FRU/0.000,0.005,0.010,0.015,0.020,0.025,0.030,0.035,
* 0.040,0.045,0.050,0.055,0.060,0.065,0.070,0.075,
* 0.080,0.085,0.090,0.095,0.100,0.110,0.120,0.130,
* 0.140,0.150,0.160,0.170,0.180,0.190,0.200,0.210,
* 0.220,0.230,0.240,0.250,0.260,0.270,0.280,0.290,
* 0.300,0.310,0.320,0.330,0.340,0.350,0.360,0.370,
* 0.380,0.390,0.400/
DATA AKP1/7.50,7.25,7.05,6.85,6.70,6.55,6.40,6.25,6.10,
* 5.95,5.80,5.70,5.60,5.49,5.42,5.34,5.27,5.20,
* 5.13,5.06,5.00,4.88,4.76,4.66,4.57,4.50,4.42,
* 4.34,4.28,4.18,4.10,4.03,3.97,3.91,3.85,3.80,
* 3.75,3.70,3.65,3.60,3.55,3.50,3.45,3.40,3.35,
* 3.30,3.26,3.23,3.20,3.17,3.15/
CALL SPLING(NI,FRU,AKP1,FRUF,RK1)
RETURN
END

```

II - 15

```

C-----
C SUBROUTINE TYDATA(SRR,SFR,HSRR)
C THIS SUB. USED TO GET INTERPOLATED DATA FROM
C BREITSCHNEIDER'S TYPHOON FORECASTING CHART.
C PARAMETER(NRR=10,NFR=9)
C RR TO BE R/R
C FRI TO BE(FR)/UR
C HRR1 TO BE HR/HR
C DIMENSION RR(NRR),HRR1(NRR,NFR),FRI(NFR),HRR2(NRR),HRR3(NFR)
DATA RR/1.,2.,3.,4.,5.,6.,7.,8.,9.,10./
DATA FRI/0.,0.02,0.04,0.06,0.1,0.16,0.2,0.3,0.5/
DATA HRR1/1.00,1.05,1.01,1.01,1.05,0.50,0.84,0.79,0.75,0.71,0.67
1 1.00,1.03,0.98,0.90,0.83,0.76,0.69,0.63,0.58,0.54
2 1.00,1.01,0.94,0.83,0.74,0.65,0.57,0.50,0.44,0.39
3 1.00,1.00,0.89,0.78,0.67,0.57,0.47,0.40,0.33,0.28
4 1.00,0.95,0.81,0.66,0.53,0.42,0.32,0.25,0.19,0.15
5 1.00,0.91,0.74,0.55,0.41,0.29,0.21,0.14,0.10,0.07
6 1.00,0.87,0.66,0.48,0.35,0.24,0.15,0.10,0.06,0.04
7 1.00,0.83,0.57,0.35,0.22,0.13,0.08,0.04,0.03,0.02
8 1.00,0.70,0.40,0.23,0.13,0.07,0.04,0.02,0.01,0.01/
DO 144 I1=1,NFR
DO 113 I2=1,NRR
HRR2(I2)=HRR1(I2,I1)
CONTINUE
113 CALL SPLING(NRR,RR,HRR2,SRR,HRR3(I1))
CONTINUE
144 CALL SPLING(NFR,FRI,HRR3,SFR,HSRR)
RETURN
END

```

```

C-----
C SUBROUTINE HT1CTANG,THANG,VF,UPS,RF,RMAX,UR,CP,DD,
C FRUF,SRR,HRM,HSRM)

```

```

C WRITE(*,*) 'TANG=',TANG
TANG=TANG+115
C WRITE(*,*) 'TANG=',TANG
TANG=ABS(TANG-TMANG)
C WRITE(*,*) 'TANG=',TANG
TANG=0.01745*TANG
DU=0.5*VF*COS(TANG)
WRITE(*,*) 'DU=',DU
URSM=URS+DU
WRITE(*,*) 'URSM=',URSM
FRUR=RF*OMAX/UR
WRITE(*,*) 'FRUR=',FRUR
CALL KPRAN(FRUR,RK1)
WRITE(*,*) 'RK1=',RK1
C HR(FT)
HR=RK1*(RMAX*DP)**0.5
WRITE(*,*) 'HR=',HR
WRITE(*,*) 'DO=',DO
SRR=DO**0.539967RMAX
WRITE(*,*) 'SRR=',SRR
CALL TYDATA(SRR,FRUR,HSRR)
WRITE(*,*) 'HSRR=',HSRR
HSR=HSRR*HR
WRITE(*,*) 'HSR=',HSR
ABI=(CURSM/URS)**2
HRM=(FT)*
HRM=HR*ABI
HSRM=(FT)*
HSRM=HSR*(CURSM/URS)**2
WRITE(*,*) 'HSRM=',HSRM
RETURN
END

```

16

```

-----
SUBROUTINE PERIOD(FRUR,SRR,UR,DU,HSRM,TSRM)
ABI=0.5*FRUR*SRR
WRITE(*,*) 'ABI=',ABI
AB2=(1.+FRUR)/SRR*EXP(1.-1./SRR)
WRITE(*,*) 'AB2=',AB2
USR=UR*(-ABI+(AB2+ABI**2)**0.5)
WRITE(*,*) 'USR=',USR
URSM=0.865*USR+DU
WRITE(*,*) 'URSM=',URSM
ABI=1.+40.*HSRM/(CURSM**2)
WRITE(*,*) 'ABI=',ABI
AB2=1.-40.*HSRM/(CURSM**2)
WRITE(*,*) 'AB2=',AB2
IF(ABI/AB2 .LE. 0.) THEN
  TSRM=0.
  GO TO 111
END IF
AB3=ALOG((ABI/AB2)**0.5)
WRITE(*,*) 'AB3=',AB3
FOI=URSM*0.4*TANH(AB3**0.6)
WRITE(*,*) 'FOI=',FOI
TSRM=(0.8)**0.25*FOI
WRITE(*,*) 'TSRM=',TSRM
RETURN
111
END

```

111

```

C-----
C SUBROUTINE SPLINGNP,X,Y,XX,YY)
C *****
C THIS PROGRAM IS USED TO INTERPOLATE A CURVE BY
C GLOBAL SPLINE CURVE.
C NP: KNOWN POINT NUMBERS
C X : X-COORDINATE OF NP POINTS
C Y : Y-COORDINATE OF NP POINTS
C XX: X-COORDINATE TO INTERPOLATE
C YY: Y-COORDINATE CORRESPONDING TO XX
C *****
C DIMENSION X(1),Y(1),A(50),B(50),D(50),H(50),
C STA(50),GMA(50),FI(50),AB(3,50)
C CAL EACH SEGMENT X COORDINATE DIFFERENCE.
C DO 12 I=1,NP-1
C H(I)=X(I+1)-X(I)
12 CONTINUE
C SOLVE SPLINE SIMULTANEOUS EQ.
C DO 13 I=2,NP-1
C A(I)=H(I-1)/H(I)
C B(I)=2.*(1+H(I-1))/H(I)
C ABS=CY(I+1)-Y(I))/H(I)
C CR=(Y(I)-Y(I-1))/H(I-1)
C D(I)=(6.-/H(I))*(ABS-CR)
13 CONTINUE
C STA(2)=B(2)
C DO 14 IJ=3,NP-1
C BTAC(IJ)=B(IJ)-A(IJ)/BTAC(IJ-1)
C GMA(2)=D(2)/B(2)
C GMA(IJ)=(D(IJ)-A(IJ)*GMA(IJ-1))/BTAC(IJ)
14 CONTINUE
C FI(NP-1)=GMA(NP-1)
C FI(1)=0.
C FI(NP)=0.
C DO 15 IL=NP-2,2,-1
C FIC(IL)=GMA(IL)-FI(IL+1)/BTAC(IL)
15 CONTINUE
C DO 17 I=1,NP-1
C IF(CX -LT. X(1)) GO TO 32
C IF(CX -GE. X(I) .AND. XX .LE. X(I+1)) GO TO 32
C IF(CX .GT. X(NP)) GO TO 50
17 CONTINUE
C GO TO 32
C I=NP-1
C PP=FI(I)*(X(I+1)-XX)**3/(6*H(I))
C QQ=FI(I+1)*(XX-X(I))**3/(6*H(I))
C RR=Y(I+1)/H(I)-H(I)*FI(I+1)/6.
C SS=RR*(XX-X(I))
C TT=Y(I)/H(I)-H(I)*FI(I)/6.
C UU=TT*(X(I+1)-XX)
C YY=PP+QQ+SS+UU
C RETURN
C END

```

H - 17



CHORNGJTWINDM.FOR

C PROGRAM TSWELL.FCR (ONLY CONSIDER SWELL OF TYPHOON).

C NG1MAX: ALLOWABLE MAX. GRID NO OF WIND FIELD.

C NG2MAX: ALLOWABLE MAX. GRID NO OF WAVE FIELD.

C NPHOON: ALLOWABLE MAX. NO. OF TYPHOON.

C PARAMETER (NG1MAX=500,NG2MAX=200,NPHOON=4)

REAL LON1,LAT1

REAL LON2(NG2MAX),LAT2(NG2MAX),LON22,LAT22

INTEGER IYY,IMM,IDD,THR,CYY,CHM,CDD,CHR,TD

DIMENSION AREA(34)

AREA: UNITS(KM\*\*2)

DATA AREA/9:0.,12141.610,12100.988,12056.530,12008.190,

11954.620,11897.050,11839.210,11778.530,11711.180,

11639.610,11566.310,11489.960,11409.170,11323.810,

11236.520,11145.880,11051.750,10954.060,10852.820,

10746.410,10638.940,10530.360,10416.390,10299.700,

10177.280/

OPENUNIT=1, FILE='WAVEGRD.DAT', STATUS='OLD')

OPENUNIT=2, FILE='TYPHOON1.DAT', STATUS='OLD')

OPENUNIT=3, FILE='TYPHOON2.DAT', STATUS='OLD')

OPENUNIT=4, FILE='TYPHOON3.DAT', STATUS='OLD')

OPENUNIT=5, FILE='TYPHOON4.DAT', STATUS='OLD')

OPENUNIT=6, FILE='TSWELL.OUT', STATUS='NEW')

OPENUNIT=10, FILE='CASTDATE.CAT', STATUS='OLD')

OPENUNIT=11, FILE='WINDGRD.DAT', STATUS='OLD')

NG1=1

REWIND 11

READ(11,\*)

33 READ(I1,\*,FNC=34) I1,LON1,LAT1

NG1=NG1+1

GO TO 33

34 NG1=NG1-1

REWIND 11

NG2=1

REWIND 1

READ(1,\*)

36 READ(I1,\*,END=37) I2,LON2(I2),LAT2(I2)

NG2=NG2+1

GO TO 36

37 NG2=NG2-1

REWIND 1

C NDATE: TIME NO FOR FORECASTING WAVE.

READ(10,\*)

NDATE=1

43 READ(10,\*,FNC=44) CYY,CHM,CDD,CHR

NDATE=NDATE+1

GO TO 43

44 NDATE=NDATE-1

REWIND 10

READ(10,\*)

READ(1,\*)

XA=100.

YA=5.

SHH=0.

STI=0.



```

1 READ(4,*,END=200)YY,TMM,TDD,THR,TLON,TLAT,PO,VF,
  R10,R7,TMANG
ELSE IF(I1.EQ.4) THEN
1 READ(5,*,END=200)YY,TMM,TDD,THR,TLON,TLAT,PO,VF,
  R10,R7,TMANG
END IF
C WRITE(*,*) 'YY',YY,'TMM=',TMM,'TDD=',TDD,'THR=',THR
C WRITE(*,*) 'TLON=',TLON,'TLAT=',TLAT
C WRITE(*,*) 'PC=',PO,'VF=',VF
C WRITE(*,*) 'R10=',R10,'R7=',R7,'TMANG=',TMANG
C CALL LONLTC(TLON,TLAT,LON2(J),LAT2(J),DD)
C WRITE(*,*) 'DD,R7=',DD,R7
IF(DD.GT.0) THEN
  DP=29.92-0.02953*PG
  WRITE(*,*) 'DP=',DP
  WRITE(*,*) 'TLAT=',TLAT
  CALL FK(TLAT,RF,RK)
  WRITE(*,*) 'RF,RK=',RF,RK
  RMAX(N,MILE)
  WAVE HEIGHT: (FT)
  WAVE PERIOD: (S)
  RMAX=R7/10.*0.53996
  WRITE(*,*) 'RMAX=',RMAX
  UR=RK*(DP**0.5)-0.5*RF*RMAX
  WRITE(*,*) 'UR=',UR
  URS=0.865*UR
  WRITE(*,*) 'URS=',URS
  CALL HT2(RF,RMAX,UR,DP,
    FRU,HRM)
  WRITE(*,*) 'HRM=',HRM
  CALL PERQ2(CURS,HRM,TRM)
  WRITE(*,*) 'TRM=',TRM
  CALL IIMCUR(YY,TMM,TDD,THR,CYY,CMM,CDD,CHR,TD)
  WRITE(*,*) 'YY,TMM,TDD,THR=',YY,TMM,TDD,THR
  WRITE(*,*) 'CYY,CMM,CDD,CHR=',CYY,CMM,CDD,CHR
  WRITE(*,*) 'TD=',TD
  WRITE(*,*) 'RMAX,URS=',RMAX,URS
  AB1=DD*TRM/(RMAX*URS)
  C1=0.9053*0.1037*AB1-0.00295*(AB1**2)
  T13=C1*TRM
  VEL=1.56*T13*3600/1000
  DIST1=VEL*TD
  WRITE(*,*) 'DIST1-DC (-):NOT REACH ',DIST1-DD
  WRITE(*,*) '???? MODIFY ????'
  IF(ABS(DIST1-DD) .GT. 50) THEN
    H13=0.
    T13=0.
    GO TO 220
  END IF
  HRM:(FT)
  H13:(M)
  WRITE(*,*) 'DD=',DD
  H13=0.11*HRM*RMAX/(DD**0.5)
  WRITE(*,*) 'VEL=',VEL
  TDI=DD/VEL
  WRITE(*,*) 'TYPHOON DATA TIME INTERVAL 6HRS'
  WRITE(*,*) 'TDI=',TDI

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5-JUN-1987 09:07

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H13=H13*((6./TDI)**0.5)
REWIND 11
READ(C11,*)
DD 135 JS=1,NG1
READ(C11,*) NPT,LONI,LATI
CALL LONLTD(TLON,TLAT,LONI,LATI,DDI)
WRITE(*,*) 'NPT,DCI,R7=',NPT,DDI,R7
IF (DDI.GT .R7) GO TO 135
WRITE(*,*) 'RMAX=',RMAX
SRR=DDI/RMAX
CALL GSPEED(FRUR,SRR,UR,URSRM)
CHANGE (LONGITUDE,LATITUDE) INTO CARTESIAN COORDINATE.
(LON,LAT.) OF CARTESIAN COORDINATE ORIGIN (XA,YA) TO BE (100,5).
CCX2: CARTESIAN X-COORDINATE OF WAVE GRID POINT.
CCY2: CARTESIAN Y-COORDINATE OF WAVE GRID POINT.
CTLON: CARTESIAN X-COORDINATE OF TYPHOON CENTER.
CTLAT: CARTESIAN Y-COORDINATE OF TYPHOON CENTER.
CALL LONLTD(XA,YA,TLON,YA,CTLON)
CALL LONLTD(XA,YA,XA,TLAT,CTLAT)
CALL ANGLE(CCX1,CCY1,CILON,CTLAT,TANG2)
CALL ANGLE(CCX2,CCY2,CTLON,CTLAT,TANG1)
TANG2=TANG2+115
TANG2=ABS(TANG2-TANG1)
TANG2=0.01745*TANG2
LATJ=INT(TLAT)
AB1=(CURSRM**COS(TANG2))**2
SUBA=SUBA+AB1*AREA(LATJ)
CALL LONLTD(XA,YA,LONI,YA,CCX1)
CALL LONLTD(XA,YA,XA,LATI,CCY1)
CALL SHELTC(LON,CTLAT,CCX1,CCY1,NCODE,MAXITR)
IF (NCODE.GT.0) GO TO 135
SUBA1=SUBA1+AB1*AREA(LATJ)
CONTINUE
WRITE(*,*) 'SUBA=',SUBA
IF(SUBA .EQ. 0.) THEN
  H13=0.
ELSE
  CE=(SUBA1/SUBA)**0.5
  H13=H13*CE
: END IF
ELSE
  H13=0.
  T13=0.
END IF
SHH=SHH+H13**2
STT=STT+T13*(H13**2)
SUBA1=0
SUBA=0
WRITE(*,*) 'SHH=',SHH
WRITE(*,*) 'STT=',STT
GO TO 220
200 CONTINUE
IF(SHH .EQ. 0.) THEN
  T13=0.
  H13=0.
  GO TO 111
END IF
WRITE(*,*) 'AFTER 200,SHH=',SHH

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\_OJAI:CHORNGJTSWELL.FOR:24

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C      WRITE(*,*) 'AFTER 200,STT=',STT
      T13=STT/SHH
      H13=SHH*0.5
111    WRITE(6,138) J,LCN2(J),LAT2(J),30.48*H13,T13
138    WRITE(6,138) J,LCN2(J),LAT2(J),30.48*H13,T13
      FORMAT(1X,I4,(1X,F10.3))
      SHH=0.
      STT=0.
      REWIND 2
      REWIND 3
      REWIND 4
      REWIND 5
120    CONTINUE
888    CONTINUE
310    FORMAT(1X,I3,1X,I4,1X,I2,1X,I2,1X,I2,1X,I2,4(1X,F10.3))
      STOP
      END

```

```

-----
C      SUBROUTINE FK(FI,RF,PK)
C      FI: INPUT LATITUDE OF TYPHOON CENTER.
C      FFI: LATITUDE ARRAY OF TYPHOON CENTER.
C      FIF: F IN CHART.
C      FIK: K IN CHART.
C      PARAMETER (N1=9)
C      DIMENSION FFI(N1),FIF(N1),FIK(N1)
C      DATA FFI/20.,22.5,25.,27.5,30.,32.5,35.,37.5,40.0/
C      DATA FIF/0.18,0.20,0.22,0.24,0.26,0.28,0.30,0.32,0.34/
C      DATA FIK/67.,67.,67.,66.,66.,66.,66.,66.,66./
C      CALL SPLING(N1,FFI,FIF,FI,RF)
C      CALL SPLING(N1,FFI,FIK,FI,PK)
C      RETURN
C      END

```

```

-----
C      SUBROUTINE KPRANCFRUR,PK1)
C      FRUR: FR/UR IN CHART
C      PARAMETER (N1=51)
C      DIMENSION FRU(N1),AKFI(N1)
C      DATA FRU/0.000,0.005,0.010,0.015,0.020,0.025,0.030,0.035,
*      0.040,0.045,0.050,0.055,0.060,0.065,0.070,0.075,
*      0.080,0.085,0.090,0.095,0.100,0.110,0.120,0.130,
*      0.140,0.150,0.160,0.170,0.180,0.190,0.200,0.210,
*      0.220,0.230,0.240,0.250,0.260,0.270,0.280,0.290,
*      0.300,0.310,0.320,0.330,0.340,0.350,0.360,0.370,
*      0.380,0.390,0.400/
C      DATA AKFI/7.50,7.25,7.05,6.85,6.70,6.55,6.40,6.25,6.10,
*      5.95,5.80,5.70,5.60,5.49,5.42,5.34,5.27,5.20,
*      5.13,5.06,5.00,4.88,4.76,4.66,4.57,4.50,4.42,
*      4.34,4.28,4.18,4.10,4.03,3.97,3.91,3.85,3.80,
*      3.75,3.70,3.65,3.60,3.55,3.50,3.45,3.40,3.35,
*      3.30,3.25,3.23,3.20,3.17,3.15/
C      CALL SPLING(N1,FRU,AKFI,FRUR,PK1)
C      RETURN
C      END

```

```

-----
C      SUBROUTINE TYDATA(SRR,SFR,HSRR)
C      THIS SUB. USED TO GET INTERPOLATED DATA FROM
C      BRETSCHNEIDER'S TYPHOON FORECASTING CHART.
C      PARAMETER(NRR=10,NFR=9)

```



```

C-----
END
SUBROUTINE GSPEED(FRUR,SRR,UR,USRSM)
  AB1=0.5*FRUR*SRR
  AB2=(1.+FRUR)/SRR*EXP(1.-1./SRR)
  USR=UR*(AB1+(AB2+AB1**2)**0.5)
  USRSM=0.865*USR
  RETURN
END
C-----
SUBROUTINE SPLING(NP,X,Y,XX,YY)
C *****
C THIS PROGRAM IS USED TO INTERPOLATE A CURVE BY
C GLOBAL SPLINE CURVE.
C NP: KNOWN POINT NUMBERS
C X : X-COORDINATE OF NP POINTS
C Y : Y-COORDINATE OF NP POINTS
C XX: X-COORDINATE TO INTERPOLATE
C YY: Y-COORDINATE CORRESPONDING TO XX
C *****
  DIMENSION X(1),Y(1),A(50),B(50),D(50),H(50),
  BTAC(50),GMA(50),FI(50),ABS(3,50)
  DO 12 I=1,NP-1
    H(I)=X(I+1)-X(I)
  12 CONTINUE
  SOLVE SPLINE SIMULTANEOUS EQ.
  DO 13 I=2,NP-1
    A(I)=H(I-1)/H(I)
    B(I)=2.*(1+H(I-1))/H(I)
    ABS=(Y(I+1)-Y(I))/H(I)
    CR=(Y(I)-Y(I-1))/H(I-1)
    D(I)=(6./H(I))*(ABS-CR)
  13 CONTINUE
  BTAC(2)=B(2)
  DO 14 IJ=3,NP-1
    BTA(IJ)=B(IJ)-A(IJ)/BTA(IJ-1)
    GMA(2)=D(2)/B(2)
    GMA(IJ)=(D(IJ)-A(IJ)*GMA(IJ-1))/BTA(IJ)
  14 CONTINUE
  FI(NP-1)=GMA(NP-1)
  FI(1)=0.
  FI(NP)=0.
  DO 15 IL=NP-2,-1
    FI(IL)=GMA(IL)-FI(IL+1)/BTA(IL)
  15 CONTINUE
  DO 17 I=1,NP-1
    IF(XX.LT.X(I)) GO TO 32
    IF(XX.GE.X(I).AND.XX.LE.X(I+1)) GO TO 32
    IF(XX.GT.X(NP)) GO TO 50
  17 CONTINUE
  GO TO 32
  50 I=NP-1
  32 PP=FI(I)*(X(I+1)-XX)**3/(6*H(I))
  QQ=FI(I+1)*(XX-X(I))**3/(6*H(I))
  RR=(Y(I+1)/H(I)-H(I)*FI(I+1))/6.
  SS=RR*(XX-X(I))
  TT=Y(I)/H(I)-H(I)*FI(I)/6.

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5-JUN-1987 09:07

\_DJAI:CHORNGJISWELL.FOR:24

UU=TI\*(X(I+1)-XX)  
YY=PP+QQ+SS+UU

RETURN  
END

C-----

6-MAY-1987 11:39

\_DJAI:CHORNGJSUMCWB.FOR:8

```

C      SUMCWB.FOR
C      THIS PROG. USED TO INTEGRATE MONSOON, TYPHOON WIND WAVE, SWELL
C      INTEGER CYY,CMM,CDD,CHR
C      CHARACTER*70 RECI,REC2,REC3
C      REAL LON2,LAT2
C      OPEN(UNIT=1,FILE='MONSCON.OUT',STATUS='OLD')
C      OPEN(UNIT=2,FILE='TWINDOW.OUT',STATUS='OLD')
C      OPEN(UNIT=3,FILE='TSWELL.OUT',STATUS='OLD')
C      OPEN(UNIT=4,FILE='CASTDATE.OAT',STATUS='OLD')
C      OPEN(UNIT=5,FILE='SUMCWB.OUT',STATUS='NEW')
C      OPEN(UNIT=6,FILE='WAVEGRD.DAT',STATUS='OLD')
C      READ(4,*)
C      NDATE=1
C      READ(4,*,END=34) CYY,CMM,CDD,CHR
C      NDATE=NDATE+1
C      GO TO 33
C      NDATE=NDATE-1
C      READ(6,*)
C      NG2=1
C      READ(6,*,END=38) NT,LON2,LAT2
C      NG2=NG2+1
C      GO TO 36
C      NG2=NG2-1
C      GO TO 36
C      DO 50 JJ=1,NDATE
C      WRITE(5,123) JJ
C      FORMAT(1,'FORECAST WAVE NO=',I2)
C      READ(1,54) RECI
C      WRITE(5,54) RECI
C      READ(1,54) REC2
C      WRITE(5,54) REC2
C      READ(1,54) REC3
C      WRITE(5,54) REC3
C      READ(2,*)
C      READ(2,*)
C      READ(2,*)
C      READ(3,*)
C      READ(3,*)
C      READ(3,*)
C      WRITE(*,*) 'FORECAST WAVE NO=',JJ
C      WRITE(*,*) RECI
C      WRITE(*,*) REC2
C      WRITE(*,*) REC3
C      DO 60 J=1,NG2
C      WRITE(*,*) 'J=',J
C      READ(1,*) NPT,LON2,LAT2,H1,T1
C      READ(2,*) NPT,LON2,LAT2,H2,T2
C      READ(3,*) NPT,LON2,LAT2,H3,T3
C      SH2=H1**2+H2**2+H3**2
C      H13=SH2**0.5
C      T13=(T1*H1**2+T2*H2**2+T3*H3**2)/SH2
C      WRITE(5,70) J,LON2,LAT2,H13,T13
C      WRITE(*,70) J,LON2,LAT2,H13,T13

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-DJAI:CHORNGJSUMCWS.FDR:8

70           FORMAT(1X,I4,4(1X,F10.3))  
60           CONTINUE  
50           CONTINUE  
54           FORMAT(A70)  
            STOP  
            END

6-MAY-1987 11:39

PAGE 2

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16-JUN-1987 14:52

\_DJA1:CHORNGJCHBL18.FDR:10

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C-----
C SUBROUTINE SHELTC(CXM,CYM,CX2,CY2,NCODE,MAXITR)
C
C (CXM,CYM): CARTESIAN COORDINATE OF MEASURING STATION.
C (CX2,CY2): CARTESIAN COORDINATE OF WIND GRID POINT.
C NCODE=1: THE MEASURE STATION IS SHELTERED.
C NCODE=0: THE MEASURE STATION IS NOT SHELTERED.
C MAXITR : MAX. ITERATION NUMBER FOR ALL SHELTERED PROCESS.
C EPS: ALLOWABLE ERROR MARGIN IN ITERATION.
C NITER: TOTAL ITERATION TIMES.

```

```

C DATA EPS/1./,NITER/10/
C MAXITR=0
C IF(CYM .EQ. CY2) THEN
C CY2=CY2*0.125
C NCY2=1
C END IF
C IF(CXM .EQ. CX2) THEN
C CX2=CX2*0.125
C NCX2=1
C END IF
C RXMIN: MIN. X VALUE OF SEGMENT OF MEASURING STATION TO WIND GRID POINT.
C RYMIN: ... Y .....
C RXMAX: MAX. X .....
C RYMAX: ... Y .....
C RXMIN=AMINI(CXM,CX2)
C RXMAX=AMAXI(CXM,CX2)
C RYMIN=AMINI(CYM,CY2)
C RYMAX=AMAXI(CYM,CY2)
C NCODE=0

```

```

C .....
C CALL TSLT1(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL MSLT2(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL HSLT3(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL KSLT4(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL JSLT5(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL JSLT6(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL JSLT7(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL PSLT8(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL PSLT9(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL PSLT10(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL PSLT11(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C * CALL PSLT12(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
C RYMIN,RYMAX,NCODE,MAXITR)
C .....
C IF(NCY2 .EQ. 1) THEN
C CY2=CY2*0.125

```

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*      1273.00,1383.69,1450.11,1516.52,1605.07,2014.62,
*      2081.03,2191.72,2247.06,2335.61,2390.95,
*      2402.02,2435.22,2435.22,2357.74,2346.68,2424.15,
*      2424.15,2414.09,2413.05,2313.47/
DATA YMIN/600.04,755.62,1144.54,1422.34,1489.01,1555.68,
1700.14,1846.59,1777.92,1711.25,1711.25,1722.36,
1766.81,1833.48,1866.82,1922.38,1955.71,1966.82,
2166.84,2222.40,2377.97,2411.30,2444.64,2577.98,
2600.21,2689.11,2778.00,2811.34,2811.34,2844.67,
2878.01,2955.79,2955.79,3066.91/
DATA YMAX/755.62,1144.54,1422.34,1489.01,1555.68,1700.14,
1866.82,1866.82,1844.59,1777.92,1722.36,1766.81,
1833.48,1866.82,1922.38,1955.71,1966.82,2166.84,
2222.40,2377.97,2411.30,2444.64,2577.98,2600.21,
2689.11,2778.00,2811.34,2811.34,2844.67,2878.01,
2966.91,2966.91,3066.91,3311.38/
C.....
CALL CROSS(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
RYMIN,RYMAX,XMIN,XMAX,YMIN,YMAX,
NLAND,NC,NCODE,MAXITR)
RETURN
END
SUBROUTINE HSLT3(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
RYMIN,RYMAX,NCODE,MAXITR)
C      THIS SUB. CHECK IF WIND GRID POINT IS SHELTERED BY HAILAND.
C      NC: CURVE NUMBERS FOR ONE LAND CONTOUR.
C      NLAND=3: REPRESENT HAILAND.
C.....
PARAMETER(NC=4)
DIMENSION XMIN(NC),XMAX(NC),YMIN(NC),YMAX(NC)
NLAND=3
C      THE FOLLOWING DATA DECLARATION ALL TO BE CARTESIAN COORDINATION.
C      THE (LONGITUDE,LATITUDE) OF CRIGION TO BE (100,5).
DATA XMIN/1173.373,1029.474,963.057,963.057/
DATA XMAX/1217.654,1173.373,1029.474,1217.654/
DATA YMIN/1600.127,1477.896,1477.896,1589.016/
DATA YMAX/1722.360,1600.127,1589.016,1722.360/
C.....
CALL CROSS(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
RYMIN,RYMAX,XMIN,XMAX,YMIN,YMAX,
NLAND,NC,NCODE,MAXITR)
RETURN
END
SUBROUTINE KSLT4(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
RYMIN,RYMAX,NCODE,MAXITR)
C      THIS SUB. CHECK IF WIND GRID POINT IS SHELTERED BY KOREA.
C      NC: CURVE NUMBERS FOR ONE LAND CONTOUR.
C      NLAND=4: REPRESENT KOREA.
C.....
PARAMETER(NC=2)
DIMENSION XMIN(NC),XMAX(NC),YMIN(NC),YMAX(NC)
NLAND=4
C      THE FOLLOWING DATA DECLARATION ALL TO BE CARTESIAN COORDINATION.
C      THE (LONGITUDE,LATITUDE) OF CRIGION TO BE (100,5).
DATA XMIN/2911.136,2933.271/
DATA XMAX/2933.271,3154.615/
DATA YMIN/3255.816,3255.816/
DATA YMAX/3311.376,3322.489/

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C.....
* CALL CROSS(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
* RYMIN,RYMAX,XMIN,XMAX,YMIN,YMAX,
* NLAND,NC,NCODE,MAXITR)
* RETURN
* END
* SUBROUTINE JSLT6(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
* RYMIN,RYMAX,NCODE,MAXITR)
* THIS SUB. CHECK IF WIND GRID POINT IS SHELTERED BY NINEZO.
* NC: CURVE NUMBERS FOR ONE LAND CONTOUR.
* NLAND=6: REPRESENT NINEZO.
C.....
* PARAMETER(NC=10)
* DIMENSION XMIN(NC),XMAX(NC),YMIN(NC),YMAX(NC)
* NLAND=6
* THE FOLLOWING DATA DECLARATION ALL TO BE CARTESIAN COORDINATION.
* THE (LONGITUDE,LATITUDE) OF CRIGION TO BE (100,5).
* DATA XMIN/3421.284,3353.819,3265.284,3265.284,3342.751,3342.751
* ,3342.751,3398.084,3486.617,3508.749/
* DATA XMAX/3508.749,3431.284,3353.819,3342.751,3353.819,3353.819
* ,3398.084,3486.617,3530.881,3530.881/
* DATA YMIN/3133.585,3189.144,3144.696,3078.025,3078.025,3011.352
* ,2900.232,2900.232,2989.129,3089.137/
* DATA YMAX/3189.144,3200.256,3200.256,3144.696,3122.472,3122.472
* ,3011.352,2989.129,3089.137,3133.585/
C.....
* CALL CROSS(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
* RYMIN,RYMAX,XMIN,XMAX,YMIN,YMAX,
* NLAND,NC,NCODE,MAXITR)
* RETURN
* END
* SUBROUTINE JSLT7(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
* RYMIN,RYMAX,NCODE,MAXITR)
* THIS SUB. CHECK IF WIND GRID POINT IS SHELTERED BY FOURGO.
* NC: CURVE NUMBERS FOR ONE LAND CONTOUR.
* NLAND=7: REPRESENT FOURGO.
C.....
* PARAMETER(NC=7)
* DIMENSION XMIN(NC),XMAX(NC),YMIN(NC),YMAX(NC)
* NLAND=7
* THE FOLLOWING DATA DECLARATION ALL TO BE CARTESIAN COORDINATION.
* THE (LONGITUDE,LATITUDE) OF CRIGION TO BE (100,5).
* DATA XMIN/3763.269,3685.808,3630.478,3564.080,3564.080,3641.542
* ,3741.138/
* DATA XMAX/3829.664,3763.269,3685.808,3630.478,3641.542,3741.138
* ,3829.664/
* DATA YMIN/3200.256,3211.368,3211.368,3155.808,3078.025,3078.025
* ,3166.919/
* DATA YMAX/3255.816,3255.816,3222.480,3222.480,3155.808,3166.919
* ,3200.256/
C.....
* CALL CROSS(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
* RYMIN,RYMAX,XMIN,XMAX,YMIN,YMAX,
* NLAND,NC,NCODE,MAXITR)
* RETURN
* END
* SUBROUTINE PSLT8(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,

```

```

C # RYMIN,RYMAX,NCODE,MAXITR)
C THIS SUB. CHECK IF WIND GRID POINT IS SHELTERED BY LIUSON.
C NC: CURVE NUMBERS FOR ONE LAND CONTOUR.
C NLAND=8: REPRESENT LIUSON.
C .....
C PARAMETER(NC=21)
C DIMENSION XMIN(NC),XMAX(NC),YMIN(NC),YMAX(NC)
C NLAND=8
C THE FOLLOWING DATA DECLARATION ALL TO BE CARTESIAN COORDINATION.
C THE (LONGITUDE,LATITUDE) OF ORIGIN TO BE (100,5).
C DATA XMIN/2247.062,2235.992,2191.719,2191.719,2269.198,2269.198
* 2269.198,2402.017,2490.562,2501.630,2590.175,2612.310
* 2612.310,2450.562,2368.813,2368.813,2468.426,2446.290
* 2446.290,2335.608,2247.062/
C DATA XMAX/2269.198,2269.198,2235.992,2269.198,2324.539,2324.539,
* 2402.017,2490.562,2501.630,2590.175,2678.717,2678.717,
* 2645.514,2645.514,2490.562,2468.426,2490.562,2490.562,
* 2468.426,2468.426,2335.608/
C DATA YMIN/1355.663,1233.432,1233.432,1044.528,1044.528,966.742,
* 966.742,900.071,900.071,888.960,877.848,877.848,
* 955.630,966.742,1022.305,1144.535,1277.880,1333.441,
* 1433.448,1500.120,1389.000/
C DATA YMAX/1389.000,1355.663,1255.656,1255.656,1055.641,1055.641,
* 988.968,988.968,977.856,977.856,888.960,888.960,955.630,
* 966.742,1022.305,1144.535,1277.880,1333.441,1433.448,
* 1500.120,1500.120,1500.120/
C .....
C CALL CROSS(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
* RYMIN,RYMAX,XMIN,XMAX,YMIN,YMAX,
* NLAND,NC,NCODE,MAXITR)
C RETURN
C END

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II - 32

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C -----
C SUBROUTINE CROSS(CXM,CYM,CX2,CY2,XA,YA,EPS,NITER,RXMIN,RXMAX,
* RYMIN,RYMAX,XMIN,XMAX,YMIN,YMAX,
* NLAND,NC,NCODE,MAXITR)
C DIMENSION XMIN(1),XMAX(1),YMIN(1),YMAX(1)
C DO 99 II=1,NC
* X=(XMIN(II)+XMAX(II))/2.
* DO 20 I=1,NITER
* XCLD=X
C .....
C IF(NLAND .EQ. 1) X=TG1(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 2) X=MG2(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 3) X=HG3(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 4) X=KG4(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 5) X=JG5(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 6) X=JG6(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 7) X=JG7(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 8) X=PG8(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 9) X=PG9(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 10) X=PG10(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 11) X=PG11(X,CXM,CYM,CX2,CY2,CX,II)
C IF(NLAND .EQ. 12) X=PG12(X,CXM,CYM,CX2,CY2,CX,II)
C .....
C IF(ABS(X-XCLD).LE.EPS .AND. X.GE.XMIN(II) .AND.
* X.LE.XMAX(II) .AND. X.GE.RXMIN .AND. X.LE.RXMAX
* .AND. CX.GE.YMIN(II) .AND. CX.LE.YMAX(II) .AND.

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16-JUN-1987 14:52

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*
CX,GE,RYMIN .AND. CX,LE,RYMAX) THEN
NCCODE=NCCODE+1
IF(I,GE,MAXITR) MAXITR=I
WRITE(*,*) NLAND = ,NLAND
WRITE(*,*) THE CURVE NO = ,II
WRITE(*,45) I
FORMAT(1,CONVERGES IN',I4,' ITERATION/')
GO TO 99

20 CONTINUE
99 CONTINUE
RETURN
END

C-----
C.....
FUNCTION TG(CX,CYM,CX2,CY2,CX,II)
CX: CURVE FITTING FUNCTION OF LAND.
PCX: THE FIRST ORDER DERIVATIVE OF FUNCTION CX.
X22=X**2
GO TO (5,10,15,20,25,30,35,40,45,50,55,60),II
5 CX=6.50775E+03-2.00605*X
PCX=-2.00605
GO TO 2
10 CX=2.70197E+03-3.37030E-01*X
PCX=-3.37030E-01
GO TO 2
15 CX=1.54557E+04-6.01274E+00*X
PCX=-6.01274E+00
GO TO 2
20 CX=1.34447E+04-5.11360E+00*X
PCX=-5.11360E+00
GO TO 2
25 CX=-1.05982E+03+1.40529E+00*X
PCX=1.40529E+00
GO TO 2
30 CX=8.14162E+02+6.02936E-01*X
PCX=6.02936E-01
GO TO 2
35 CX=4.64754E+03-1.00038E+00*X
PCX=-1.00038E+00
GO TO 2
40 CX=1.62185E+04-5.00814E+00*X
PCX=-5.00814E+00
GO TO 2
45 CX=-2.69360E+03+2.00360E+00*X
PCX=2.00960E+00
GO TO 2
50 CX=-5.87323E+03+3.33942E+00*X
PCX=3.33942E+00
GO TO 2
55 CX=-1.94951E+03+1.67521E+00*X
PCX=1.67521E+00
GO TO 2
60 CX=-3.89087E+03+2.51038E+00*X
PCX=2.51038E+00
C.....
YX21=(CY2-CYM)/(CX2-CXM)

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16-JUN-1987 14:52

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C FX: THE ROOT OF EQUATION FX=0 REPRESENTS THE INTERSECTION POINT  
C BETWEEN CX AND LINE OF MEASURING STATION TO WIND GRID POINT.

C FX=CX-YX21\*(CX-CXM)-CYM

C PFX: THE FIRST ORDER DERIVATIVE OF FUNCTION FX.

PFX=PCX-YX21

C.....TG1=X-FX/PFX

C.....RETURN

END

-----

C FUNCTION MG2CX,CXM,CYM,CX2,CY2,CX,II)

C CX: CURVE FITTING FUNCTION OF LAND.

C PCX: THE FIRST ORDER DERIVATIVE OF FUNCTION CX.

X22=X\*\*2

X33=X\*\*3

GO TO (5,10,15,20,25,30,35,40,45,50,55,60,65,70,75,80,85,  
90,95,100,105,110,115,120,125,130,135,140,145,150,  
155,160,165,170),II

CX=1.6930E+03-2.9405\*\*X+1.9791E-03\*\*X22

PCX=-2.9405+3.9582E-03\*\*X

GO TO 2

CX=1.7272E+03+1.2087\*\*X-2.0058E-03\*\*X22

PCX=1.2087-4.0116E-03\*\*X

GO TO 2

CX=2.3581E+03-1.3209\*\*X

PCX=-1.3209

GO TO 2

CX=-1.917E+05+5.6574E+02\*\*X-4.1390E-01\*\*X22

PCX=5.6574E+02-0.8278\*\*X

GO TO 2

CX=2.489E+03-1.5056\*\*X

PCX=-1.5056

GO TO 2

CX=-1.0361E+04+3.4527E+01\*\*X-2.469E-02\*\*X22

PCX=3.4527E+01-0.04938\*\*X

GO TO 2

CX=2.9264E+02+3.0136\*\*X-1.444E-03\*\*X22

PCX=3.0136-2.888E-03\*\*X

GO TO 2

CX=-5.1761E+04+1.0429E+02\*\*X-5.0664E-02\*\*X22

PCX=1.0429E+02-0.10133\*\*X

GO TO 2

CX=-4.6195E+03+6.0201\*\*X

PCX=6.0201

GO TO 2

CX=4.781E+04-8.279E+01\*\*X+3.7231E-02\*\*X22

PCX=-8.28779E+01+0.074466\*\*X

GO TO 2

CX=1.1389E+03+5.0201E-01\*\*X

PCX=5.0201E-01

GO TO 2

CX=4.057E+03-2.0086\*\*X

PCX=-2.0086

GO TO 2

CX=-4.0149E+03+9.305\*\*X-3.7014E-03\*\*X22

PCX=9.305-7.4028E-03\*\*X

GO TO 2



651

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70 CX=-5.945E+03+1.1457E+01\*X-4.1994E-03\*\*X22  
 PCX=1.1457E+01-8.3988E-03\*\*X  
 GO TO 2

75 CX=-2.6099E+03+5.6595\*X-1.7532E-03\*\*X22  
 PCX=5.6595-3.5064E-03\*\*X  
 GO TO 2

80 CX=-4.6768E+04+6.5347E+01\*X-2.1914E-02\*\*X22  
 PCX=6.5347E+01-0.04383\*\*X  
 GO TO 2

85 CX=1.3355E+05-1.6895E+02\*X+5.4198E-03\*\*X22  
 PCX=-1.6896E+02+0.1084\*\*X  
 GO TO 2

90 CX=6.5286E+03-5.4731\*\*X+1.6393E-03\*\*X22  
 PCX=-5.4731+3.2786E-03\*\*X  
 GO TO 2

95 CX=8.122E+04-7.8018E+01\*X+1.9248E-02\*\*X22  
 PCX=-7.8018E+01+0.0385\*\*X  
 GO TO 2

100 CX=1.1250E+04-9.8082\*\*X+2.6257E-03\*\*X22  
 PCX=-9.8082+5.2514E-03\*\*X  
 GO TO 2

105 CX=8.9047E+03-2.9778\*\*X  
 PCX=-2.9778  
 GO TO 2

110 CX=-3.058E+05+2.7798E+02\*\*X-6.2667E-02\*\*X22  
 PCX=2.7798E+02-0.1253\*\*X  
 GO TO 2

115 CX=-9.3956E+02+1.5061\*\*X  
 PCX=1.5061  
 GO TO 2

120 CX=-5.5478E+02+2.2652\*\*X-3.9569E-04\*\*X22  
 PCX=2.2652-7.9138E-04\*\*X  
 GO TO 2

125 CX=-1.772E+03+6.7132E-01\*X+4.9051E-04\*\*X22  
 PCX=6.7132E-01+9.8102E-04\*\*X  
 GO TO 2

130 CX=-1.2349E+03+8.2977E-01\*X+3.3328E-04\*\*X22  
 PCX=8.2977E-01+6.6656E-04\*\*X  
 GO TO 2

135 CX=2.4989E+03+6.8019E-01\*X-2.3247E-04\*\*X22  
 PCX=6.8019E-01-4.6494E-04\*\*X  
 GO TO 2

140 CX=8.2498E+03-4.7371\*\*X+1.0305E-03\*\*X22  
 PCX=-4.7371+2.061E-03\*\*X  
 GO TO 2

145 CX=6.2195E+01+2.025\*\*X-3.576E-04\*\*X22  
 PCX=2.025-7.152E-04\*\*X  
 GO TO 2

150 CX=-1.8255E+03+3.4929\*\*X-6.4062E-04\*\*X22  
 PCX=3.429-1.2812E-03\*\*X  
 GO TO 2

155 CX=1.9134E+03+1.8377\*\*X-5.9132E-04\*\*X22  
 PCX=1.8377-1.1826E-03\*\*X  
 GO TO 2

160 CX=3.3612E+03-1.6802E-01\*\*X  
 PCX=-1.6802E-01  
 GO TO 2

165 CX=-2.4782E+04+2.4486E+01\*X-5.3607E-03\*\*X22

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PCX=2.4486E+01-1.0761E-02*X
GO TO 2
CX=-2.024E+04+9.887*X+5.9886E-03*X2-2.5531E-06*X33
PCX=9.887+1.1977E-02*X-7.6593E-06*X22
C.....
2 YX21=(CY2-CYM)/(CX2-CXM)
C FX: THE ROOT OF EQUATION FX=0 REPRESENTS THE INTERSECTION POINT
C BETWEEN CX AND LINE OF MEASURING STATION TO WIND GRID POINT.
C FX=CX-YX21*(X-CXM)-CYM
C PFX: THE FIRST ORDER DERIVATIVE OF FUNCTION FX.
C PFX=PCX-YX21

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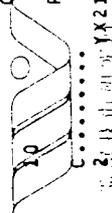
C..... MG2=X-FX/PFX
C..... RETURN
C..... END
C.....
C..... FUNCTION HG3(CX,CXM,CYM,CX2,CY2,CX,II)
C CX: CURVE FITTING FUNCTION OF LAND.
C PCX: THE FIRST ORDER DERIVATIVE OF FUNCTION CX.
X22=X**2
GO TO (5,10,15,20),II
CX=-1.0276E+03+2.7043*X-3.9617E-04*X22
PCX=2.7043-7.9234E-04*X
GO TO 2
CX=1.4385E+04-2.4086E+01*X+1.1224E-02*X22
PCX=-2.4086E+01+0.02245*X
GO TO 2
CX=3.2185E+04-6.0351E+01*X+2.9644E-02*X22
PCX=-6.0351E+01+0.05929*X
GO TO 2
CX=2.9224E+02+2.0137*X-6.9034E-04*X22
PCX=2.0137-1.3807E-03*X

```

```

C.....
2 YX21=(CY2-CYM)/(CX2-CXM)
C FX: THE ROOT OF EQUATION FX=0 REPRESENTS THE INTERSECTION POINT
C BETWEEN CX AND LINE OF MEASURING STATION TO WIND GRID POINT.
C FX=CX-YX21*(X-CXM)-CYM
C PFX: THE FIRST ORDER DERIVATIVE OF FUNCTION FX.
C PFX=PCX-YX21
C..... MG3=X-FX/PFX
C..... RETURN
C..... END
C.....
C..... FUNCTION KG4(CX,CXM,CYM,CX2,CY2,CX,II)
C CX: CURVE FITTING FUNCTION OF LAND.
C PCX: THE FIRST ORDER DERIVATIVE OF FUNCTION CX.
X22=X**2
GO TO (5,10),II
CX=1.0663E+04-2.5251*X
PCX=-2.5251
GO TO 2
CX=-4.1427E+03+4.5928*X-7.0553E-04*X22
PCX=4.5928-1.4111E-03*X

```





```

PCX=-7.4783+3.8466E-03*X
GC TO 2
CX=2.6619E+04-2.2131E+01*X+4.7707E-03*X22
PCX=-2.2131E+01+9.5414E-03*X
GO TO 2
CX=1.2097E+04-8.1711*X+1.478E-03*X22
PCX=-8.1711+2.956E-03*X
GO TO 2
CX=-1.6683E+04+7.0599*X
PCX=7.0599
GO TO 2
CX=-5.0065E+04-4.1055E+01*X+8.2543E-03*X22
PCX=4.1055E+01-0.01651*X
GO TO 2
CX=2.2069E+04-1.5963E+01*X+3.0053E-03*X22
PCX=-1.5963E+01+6.0106E-03*X
GO TO 2
CX=-7.9174E+02+2.3377*X-6.4029E-04*X22
PCX=2.3377-1.2806E-03*X
GO TO 2
CX=8.0373E+01+3.3505E-01*X
PCX=3.3505E-01
GO TO 2
CX=-7.5312E+03+7.023*X-1.4403E-03*X22
PCX=7.023-2.8806E-03*X
GO TO 2
CX=1.5906E+04-1.1246E+01*X+2.1109E-03*X22
PCX=-1.1246E+01+4.2218E-03*X
GO TO 2
CX=1.8376E+03-1.7195*X+6.0504E-04*X22
PCX=-1.7195+1.2101E-03*X
GC TO 2
CX=-4.9298E+03+2.5148*X
PCX=2.5148
GO TO 2
CX=-8.7014E+03+1.0202E+01*X-2.4791E-03*X22
PCX=1.0202E+01-4.9382E-03*X
GO TO 2
CX=-5.9147E+03+3.0038*X
PCX=3.0038
GO TO 2
CX=1.3558E+04-5.3534*X-1.8308E-03*X22+8.1866E-07*(X**3)
PCX=-5.3534-3.6616E-03*X+2.4560E-06*X22
GO TO 2
CX=6.9695E+03-6.0591*X+1.5952E-03*X22
PCX=-6.0591+3.1904E-03*X

```

II - 40

```

C.....
2 YX21=(CY2-CYM)/(CX2-CXM)
C FX: THE ROOT OF EQUATION FX=0 REPRESENTS THE INTERSECTION POINT
C BETWEEN CX AND LINE OF MEASURING STATION TO WIND GRID POINT.
C FX=CX-YX21*(CX-CXM)-CYM
C PFX: THE FIRST ORDER DERIVATIVE OF FUNCTION FX.
PFX=PCX-YX21
C.....
PC8=X-FX/PFX
C.....

```

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```

C-----
C SUBROUTINE ANGLE(CXM,CYM,CX2,CY2,ANG)
C ANG: DIRECTION ANGLE (DEGREES, WITH + X AXIS) OF THE LINE FROM
C WIND GRID POINT TO MEASURING STATION.
C (CXM,CYM): COORDINATE OF MEASURING STATION.
C (CX2,CY2): COORDINATE OF WIND GRID POINT.
C DX=CXM-CX2
C DY=CYM-CY2
C IF(CX .GT. 0 .AND. DY .GT. 0) THEN
C   ANG=57.29578*ATAN(DY/DX)
C ELSE IF(CX .LT. 0 .AND. DY .GT. 0) THEN
C   ANG=57.29578*ATAN(DY/DX)+180.
C ELSE IF(CX .LT. 0 .AND. DY .LT. 0) THEN
C   ANG=57.29578*ATAN(DY/DX)+180.
C ELSE IF(CX .GT. 0 .AND. DY .LT. 0) THEN
C   ANG=57.29578*ATAN(DY/DX)+360.
C ELSE IF(CX .EQ. 0 .AND. DY .GT. 0) THEN
C   ANG=90.
C ELSE IF(CX .EQ. 0 .AND. DY .LT. 0) THEN
C   ANG=270.
C ELSE IF(CX .EQ. 0 .AND. DY .EQ. 0) THEN
C   ANG=0.

```

END IF  
RETURN  
END

```

C-----
C SUBROUTINE LONLTC(XA,YA,XB,YB,DIST)
C XA: LONGITUDE OF POINT A.
C YA: LATITUDE OF POINT A.
C XB: LONGITUDE OF POINT B.
C YB: LATITUDE OF POINT B.
C DIST: DISTANCE (KM) FROM POINT A TO POINT B.
C XAB=(ABS(XA-XB))*0.0174533
C YAB=(90-YA)*0.0174533
C YBB=(90-YB)*0.0174533
C DO=COS(XAB)*SIN(YA)*SIN(YB)+COS(YA)*COS(YB)
C IF(DO .GT. 1.0) THEN
C   DIST=0.
C ELSE
C   DIST=6366.710054*ACOS(DO)

```

END IF  
RETURN  
END

```

C-----
C SUBROUTINE TIMOUR(NYY,NMON,NDD,NHR,KYY3,KMON3,KDD3,KHR3,TD)
C NYY: YEAR(WERTERN, EX:1987) OF 1ST DATE.
C NMON: MONTH OF 1ST DATE.
C NDD: DAY OF 1ST DATE.
C NHR: HOUR OF 1ST DATE.
C KYY3: YEAR(WERTERN, EX:1987) OF 2ND DATE.
C KMON3: MONTH OF 2ND DATE.
C KDD3: DAY OF 2ND DATE.
C KHR3: HOUR OF 2ND DATE.
C TD: TIME DURATION (HR) BETWEEN 1ST DATE AND 2ND DATE.
C DIMENSION MDC(12)
C INTEGER TD1,TD2,TD

```

\_DJAI:EHORNGJWBLIB.FOR:10

```

MD(1)=31
MD(3)=31
MD(4)=30
MD(5)=31
MD(6)=30
MD(7)=31
MD(8)=31
MD(9)=30
MD(10)=31
MD(11)=30
MD(12)=31
A4=MOD(NYY,4)
A100=MOD(NYY,100)
A400=MOD(NYY,400)
IF ((A4 .EQ. 0 .AND. A100 .EQ. 0 .AND. A400 .EQ. 0) .OR.
    (A4 .EQ. 0 .AND. A100 .NE. 0)) THEN
* THIS YEAR TO BE LEAP YEAR.
  MD(2)=29
  LNY=1
ELSE
C THIS YEAR TO BE ORDINARY YEAR.
  MD(2)=28
  LNY=2
END IF
DO 100 K=1,NMON-1
  TD1=TD1+MD(K)
CONTINUE
TD1=24*(TD1+MOD-1)+NHR
A4=MOD(KYY3,4)
A100=MOD(KYY3,100)
A400=MOD(KYY3,400)
IF ((A4 .EQ. 0 .AND. A100 .EQ. 0 .AND. A400 .EQ. 0) .OR.
    (A4 .EQ. 0 .AND. A100 .NE. 0)) THEN
* THIS YEAR TO BE LEAP YEAR.
  MD(2)=29
  LNY3=1
ELSE
C THIS YEAR TO BE ORDINARY YEAR.
  MD(2)=28
  LNY3=2
END IF
DO 200 K=1,KMON3-1
  TD2=TD2+MD(K)
CONTINUE
TD2=24*(TD2+MOD3-1)+KHR3
IF(KYY3-NYY .EQ. 1 .AND. LNY .EQ. 1) TD2=366*24+TD2
IF(KYY3-NYY .EQ. 1 .AND. LNY3 .EQ. 2) TD2=365*24+TD2
TD=TD2-TD1
RETURN
END
C.....

```



附錄 III 颱風資料

颱風名	年	月	日	時	北緯	東經	中心氣壓
HAL	1985	6	19	14	16.0	132.8	997
				20	16.0	132.8	997
			20	2	16.0	132.8	997
				8	15.0	130.6	984
				14	15.2	129.8	979
				20	15.5	128.8	976
			21	2	15.9	127.8	975
				8	16.3	126.8	969
				14	16.9	125.6	969
				20	17.9	124.2	965
			22	2	18.7	122.8	965
				8	19.1	121.3	965
				14	19.3	120.3	965
				20	19.7	119.7	965
			23	2	20.4	119.0	960
				8	21.1	117.9	955
				14	21.4	116.9	960
				20	21.7	116.1	965
			24	2	21.8	115.4	965
				8	22.1	115.3	970
	14	22.8	115.3	975			
	20	23.3	115.1	975			
25	2	23.9	115.1	980			

颱風名	年	月	日	時	北緯	東經	中心氣壓			
IRMA	1985	6	27	8	15.0	130.1	988			
				14	15.8	129.9	985			
				20	16.7	129.7	980			
			28	2	17.7	129.6	975			
				8	18.8	129.7	975			
				14	20.0	129.9	965			
				20	21.3	129.9	965			
				29	2	22.9	130.0	960		
					8	24.3	130.2	957		
			14		25.7	130.2	957			
			30	20	26.9	130.5	965			
				2	28.2	131.0	965			
				8	29.5	131.8	970			
				14	30.9	133.4	970			
				20	32.4	135.5	970			
				7	1	2	34.8	138.7	970	
			NELSON	1985	8	18	8	21.0	139.8	990
							14	21.7	139.4	990
20	22.4	138.5					985			
19	2	22.6				137.5	980			
	8	22.7				136.6	979			
	14	22.9				135.8	979			
20	20	23.0				134.9	975			
	2	23.1				134.0	975			
	8	23.1				133.1	975			
21	14	23.1				132.4	971			
	20	23.2				131.6	970			
	2	23.3				131.0	970			

颱風名	年	月	日	時	北緯	東經	中心氣壓
				8	23.7	130.2	970
				14	24.0	129.0	966
				20	24.1	128.0	966
			22	2	24.2	126.9	961
				8	24.5	125.8	963
				14	24.7	124.7	963
				20	24.8	123.8	963
			23	2	25.4	122.8	965
				8	25.5	121.6	965
				14	25.6	120.6	965
				20	25.6	119.8	965
			24	2	25.5	118.4	980
BRENDA	1985	9	30	8	16.5	131.0	999
				14	16.0	131.1	995
				20	15.9	130.3	996
		10	1	2	16.1	130.1	994
				8	16.2	129.9	991
				14	17.2	129.6	989
				20	17.8	129.2	985
			2	2	17.7	128.8	995
				8	17.5	129.0	980
				14	18.3	128.0	980
				20	18.5	127.4	980
			3	2	19.1	126.1	980
				8	19.5	125.6	966
				14	20.6	124.3	964
				20	21.7	123.5	964
			4	2	22.8	123.0	964

颱風名	年	月	日	時	北緯	東經	中心氣壓
BRENDA	1985	10		8	24.7	122.9	964
				14	26.3	122.6	964
				20	27.6	123.5	967
			5	2	29.7	124.3	970
				8	31.8	126.0	970
				14	33.8	128.0	985
				20	35.6	130.5	990
DOT	1985	10	13	14	10.9	146.6	997
				20	11.2	145.1	995
			14	2	11.4	143.6	993
				8	11.6	142.5	992
				14	11.8	141.3	990
			15	20	12.2	140.1	982
				2	12.7	139.0	982
				8	13.1	137.9	969
			16	14	13.4	136.7	953
				20	13.6	135.6	945
				2	13.8	134.9	935
				8	14.1	133.7	935
				14	14.6	132.4	930
			17	20	14.6	131.2	897
				2	14.7	130.0	897
				8	14.6	128.5	897
				14	14.5	127.4	897
20	14.3	126.3		897			
18	2	14.3	125.3	897			
	8	14.5	124.3	915			
	14	14.6	123.4	926			

颱風名	年	月	日	時	北緯	東經	中心氣壓
				20	15.1	122.3	926
SARAH	1986	7	31	2	15.4	129.0	999
				8	15.5	127.9	998
				14	15.8	127.0	998
				20	16.5	125.6	994
		8	1	2	17.0	124.5	990
				8	17.0	124.6	993
				14	17.3	123.8	992
				20	17.6	123.0	992
			2	2	17.8	122.3	992
				8	17.8	122.3	992
				14	18.0	123.0	992
				20	18.1	123.5	992
			3	2	20.3	126.5	990
				8	20.5	127.5	990
				14	21.3	128.2	990
				20	23.2	130.0	985
			4	2	24.6	131.6	985
				8	27.0	135.8	985
				14	30.2	138.1	985
				20	33.5	139.3	985
			5	2	35.5	141.0	983
VERA	1986	8	13	20	16.7	132.0	998
			14	2	17.0	132.0	998
				8	17.5	131.5	997
				14	17.0	132.0	998
				20	17.9	129.8	996
			15	2	18.3	128.8	996

颱風名	年	月	日	時	北緯	東經	中心氣壓
				8	18.4	128.5	995
				14	18.4	128.2	992
				20	18.5	128.0	992
		16		2	18.6	128.0	992
				8	18.6	129.5	990
				14	19.1	129.3	990
				20	19.1	129.1	988
		17		2	19.0	129.1	988
				8	18.5	129.5	988
				14	19.1	130.9	990
				20	19.7	132.2	993
		18		2	20.3	136.5	987
				8	22.6	136.0	980
				14	22.9	136.5	980
				20	23.2	137.5	980
		19		2	23.9	138.0	985
				8	23.9	138.0	985
				14	23.4	137.7	985
				20	23.2	137.9	985
		20		2	22.0	140.2	985
				8	21.7	141.5	970
				14	21.7	141.9	965
				20	21.7	142.5	963
		21		2	21.9	143.1	963
				8	21.3	143.3	960
				14	21.5	144.1	948
				20	21.8	144.7	944
		22		2	21.8	144.9	940

颱風名	年	月	日	時	北緯	東經	中心氣壓
				8	22.0	145.5	932
				14	22.2	145.7	923
				20	22.2	145.7	925
			23	2	22.2	145.5	930
				8	22.3	144.5	930
				14	22.3	143.5	935
				20	22.3	142.4	935
			24	2	22.2	140.9	935
				8	22.1	140.0	935
				14	22.5	138.5	935
				20	22.9	136.9	935
			25	2	23.4	135.4	940
				8	24.0	133.5	950
				11	24.1	132.8	950
				14	24.3	132.0	950
				17	24.6	131.7	950
				20	24.9	130.7	950
				23	25.1	129.7	950
			26	2	25.3	128.8	950
				5	25.5	128.1	950
				8	26.0	127.4	950
				11	26.2	126.8	950
				14	26.5	126.3	955
				17	26.9	125.5	955
				20	27.2	124.8	955
			27	2	27.6	124.2	955
				8	28.6	123.5	955
				14	29.6	123.7	955

颱風名	年	月	日	時	北緯	東經	中心氣壓
				20	30.8	124.0	960
			28	2	32.4	124.4	960
				8	33.9	125.8	965
				14	35.6	125.9	965
				20	37.5	127.0	965
ABBY	1986	9	13	20	12.2	144.7	996
			14	2	13.1	143.8	996
				8	14.0	140.0	996
				14	15.0	139.0	995
				20	15.4	136.2	990
		15		2	15.9	135.2	990
				8	16.5	134.4	985
				14	17.4	133.0	985
				20	18.1	131.7	985
		16		2	18.5	130.7	980
				8	19.0	130.0	975
				14	19.6	128.9	975
				20	19.3	128.1	970
		17		2	19.0	127.2	970
				8	19.8	126.8	965
				14	20.4	125.8	953
				20	20.7	125.8	953
		18		2	20.9	124.9	953
				8	21.2	124.2	953
				14	21.8	123.3	950
				20	22.2	122.5	945
		19		2	22.7	121.9	945
				8	23.2	121.1	950

颱風名	年	月	日	時	北緯	東經	中心氣壓
				14	23.9	121.0	950
				20	24.3	120.3	960
		20		2	25.2	120.5	970
				8	26.1	121.4	982
				14	27.0	122.8	985
				20	29.0	123.4	990
		21		2	31.5	125.5	997

年	月	日	時	分	H <sub>3</sub> (米)	T <sub>3</sub> (秒)	站
			21	0	2.70	12.33	B
		29	0	0	2.24	10.93	"
			3	0	1.96	10.86	"
			6	0	1.68	11.50	"
			9	0	2.14	11.15	"
			12	0	2.24	10.84	"
			15	0	1.90	10.47	"
			18	0	1.64	9.64	"
			21	0	1.48	9.44	"
		30	0	0	1.12	8.67	"
			3	0	1.05	8.69	"
			6	0	0.96	8.73	"
			9	0	1.01	8.98	"
1985	8	21	0	0	1.30	10.74	A
			15	0	1.31	10.47	"
			16	4	1.60	10.99	"
			17	8	1.57	10.03	"
			18	12	1.87	11.39	"
			19	0	1.61	11.36	"
			20	4	1.47	10.55	"
			21	8	1.60	10.25	"
			22	12	1.90	11.54	"
			23	0	1.77	10.39	"
			23	48	2.13	10.26	"
		22	0	4	2.13	9.91	"
			1	8	1.95	9.97	"
			2	12	1.76	9.18	"
			3	0	1.77	10.14	"

附錄 IV 蘇澳波浪資料

年	月	日	時	分	$H\frac{1}{3}$ (米)	$T\frac{1}{3}$ (秒)	站
1985	6	21	6	0	1.24	8.89	B
			9	0	1.26	9.29	"
			12	0	1.46	9.77	"
			15	0	1.54	9.74	"
			18	0	1.72	10.28	"
			21	0	2.10	10.32	"
		22	0	0	2.85	11.63	"
			3	0	3.43	11.72	"
			6	0	3.83	13.23	"
			9	0	6.06	13.86	"
			12	0	6.43	13.41	"
			15	0	6.11	12.81	"
			18	0	4.82	12.60	"
			21	0	4.18	10.69	"
		23	0	0	3.96	9.00	"
			3	0	3.47	9.04	"
			6	0	3.73	9.93	"
			9	0	3.15	8.91	"
			12	0	3.25	8.73	"
			15	0	3.20	9.55	"
			18	0	2.44	7.91	"
			21	0	2.39	8.64	"
		24	0	0	2.50	8.87	"
			3	0	2.46	8.32	"
6		28	12	0	1.41	9.22	"
			15	0	1.38	9.24	"
			18	0	1.66	10.37	"

年	月	日	時	分	H <sub>3</sub> (米)	T <sub>3</sub> (秒)	站
			14	54	1.96	9.43	A
			15	58	2.31	9.56	"
			17	2	2.77	9.13	"
			18	6	2.16	9.09	"
			19	10	2.72	9.54	"
			20	14	2.22	10.03	"
			21	2	2.23	8.81	"
			22	6	1.83	8.72	"
			23	10	2.05	9.27	"
			23	58	2.05	9.44	"
		24	0	14	1.78	8.70	"
			1	2	2.16	8.98	"
			2	4	2.19	9.02	"
			3	8	2.26	8.69	"
1985	8	24	3	56	2.03	8.67	"
			5	0	2.46	8.75	"
	10	3	14	7	2.79	10.65	B
			15	59	3.32	10.28	"
			18	7	3.81	11.86	"
			19	59	5.20	12.37	"
			20	47	7.08	14.04	"
			21	35	5.97	14.30	"
			21	51	6.69	15.23	"
			22	7	6.11	14.73	"
			22	39	6.77	15.24	"
			23	11	7.58	15.93	"
			23	43	7.44	15.49	"

年	月	日	時	分	$H_{\frac{1}{3}}$ (米)	$T_{\frac{1}{3}}$ (秒)	站
			4	4	1.83	11.24	"
			5	8	1.56	9.71	"
			6	12	1.91	9.91	"
			7	0	1.80	10.08	"
			8	4	2.07	10.33	"
			9	8	1.94	9.44	"
			10	12	2.30	11.01	"
			11	0	2.30	10.88	"
			12	4	2.98	10.66	"
			13	8	2.72	10.81	"
			13	40	2.76	11.65	"
			13	59	3.41	11.06	"
			15	3	2.79	10.23	"
			16	7	3.44	10.63	"
			16	55	3.46	11.28	"
			17	59	3.87	11.71	"
			19	3	3.63	12.37	"
			20	7	4.10	11.77	"
			20	55	4.35	12.60	"
			21	59	4.54	12.58	"
			23	3	4.66	12.60	"
			23	51	4.85	12.94	"
	23		0	7	4.72	12.06	"
			0	55	4.84	12.38	"
			1	59	4.49	11.91	"
			3	3	3.94	11.42	"
			3	57	3.24	10.66	"
			9	57	1.73	8.90	"

年	月	日	時	分	$H_{\frac{1}{3}}$ (米)	$T_{\frac{1}{3}}$ (秒)	站
			23	59	8.23	15.32	"
		4	0	15	6.74	15.08	"
			1	3	5.74	14.09	"
			2	7	7.09	14.99	"
			3	11	7.69	16.31	"
			4	15	6.42	15.06	"
			5	3	7.98	15.25	"
			6	7	8.63	14.81	"
			7	11	7.41	15.63	"
			7	59	6.51	14.25	"
			8	47	4.88	14.08	"
			9	8	6.40	13.72	"
			9	56	4.53	11.87	"
			11	0	4.97	12.52	"
			12	4	4.04	10.97	"
			13	8	3.66	10.62	"
			14	12	3.51	9.79	"
			15	0	3.19	10.05	"
			16	4	3.62	10.35	"
			17	8	2.65	10.06	"
			18	12	2.93	9.02	"
			19	0	2.07	9.33	"
			20	4	2.22	11.29	"
			21	8	1.99	11.07	"
			22	12	1.92	9.52	"
			23	0	2.09	9.47	"
			23	48	2.14	9.33	"
		5	0	4	2.19	8.87	"
			2	12	1.54	9.22	"

年	月	日	時	分	$H_{\frac{1}{3}}$ (米)	$T_{\frac{1}{3}}$ (秒)	站
			3	0	1.86	9.55	"
			4	4	1.66	9.38	"
			5	8	2.35	9.55	"
			5	56	2.20	9.25	"
			7	0	2.12	8.94	"
			8	4	1.84	8.87	"
			9	8	2.13	8.47	"
			9	56	2.53	8.58	"
			10	44	2.02	8.33	"
		18	0	0	1.67	10.25	"
			3	0	2.41	10.69	"
			6	0	2.40	10.91	"
			12	0	2.38	9.37	"
			21	0	1.97	9.74	"
		19	0	0	2.33	11.09	"
			6	0	2.45	11.83	"
			12	0	1.84	10.40	"
			15	0	1.50	10.66	"
			18	0	1.85	10.64	"
			21	0	1.78	7.91	"
		20	0	0	1.95	8.24	"
			3	0	1.83	7.81	"
			6	0	1.76	8.87	"
			9	0	1.73	8.67	"
			12	0	1.60	8.22	"
			15	0	1.53	8.23	"
			18	0	1.45	7.29	"
		21	0	0	1.47	7.94	"
			9	0	1.37	7.53	"

年	月	日	時	分	H <sub>1/3</sub> (米)	T <sub>1/3</sub> (秒)	站
			21	0	1.52	7.89	"
1985	10	22	6	0	1.24	7.22	"
			12	0	1.46	8.40	"
			21	0	1.74	6.75	"
1986	8	2	4	0	2.33	9	
			5	0	2.17	9	
			6	0	2.06	9	
			7	0	1.61	8	
			8	0	1.75	8	
			9	0	1.82	8	
			10	0	1.70	8	
			11	0	2.34	7	
			12	0	2.04	8	
			13	0	2.04	8	
			14	0	2.47	9	
			15	0	2.40	9	
			16	0	2.74	9	
			17	0	2.55	9	
			18	0	2.24	8	
			19	0	2.57	9	
			20	0	2.46	9	
			21	0	2.26	9	
			22	0	2.77	9	
			23	0	2.85	10	
		3	0	0	2.99	9	
			1	0	2.93	9	
			2	0	2.41	9	
			3	0	2.57	9	
			4	0	2.48	10	

年	月	日	時	分	$H_{\frac{1}{3}}$ (米)	$T_{\frac{1}{3}}$ (秒)
			5	0	2.80	9
			6	0	1.92	9
			7	0	2.66	10
			8	0	2.64	10
			9	0	1.96	9
		17	0	0	2.31	9
			5	0	1.72	9
			7	0	2.25	10
			9	0	1.78	9
			11	0	2.19	10
			13	0	2.03	10
			15	0	2.23	10
			17	0	1.81	9
			19	0	1.67	9
			23	0	2.07	9
		18	4	0	1.83	10
			7	0	2.04	10
			13	0	1.86	10
			16	0	1.67	9
			21	0	1.36	9
		19	0	0	1.72	11
			4	0	1.34	10
			7	0	1.34	9
			8	0	1.60	10
			9	0	1.71	13
			10	0	1.39	10
			14	0	1.21	10
			16	0	1.44	11
			19	0	1.29	10

年	月	日	時	分	$H\frac{1}{3}$ (米)	$T\frac{1}{3}$ (秒)
			20	0	1.47	9
			22	0	2.03	12
	20		3	0	1.45	10
			10	0	1.29	11
			12	0	1.02	9
			13	0	1.19	9
	25		2	0	1.81	9
			4	0	1.92	10
			5	0	1.68	9
			7	0	1.93	10
			9	0	1.51	9
			10	0	1.52	9
			11	0	1.73	9
			12	0	1.49	10
			13	0	1.65	9
			14	0	1.62	10
			20	0	1.48	9
			22	0	1.22	9
			23	0	1.59	12
	26		0	0	1.53	12
			1	0	1.55	12
			1	40	1.79	13
			2	20	2.02	13
			4	0	1.86	12
			5	0	1.97	12
			6	0	2.18	12
			7	0	2.11	13
			7	40	3.00	14
			9	0	2.98	13

年	月	日	時	分	$H\frac{1}{3}$ (米)	$T\frac{1}{3}$ (秒)
			10	40	2.08	12
			12	20	2.33	11
			13	0	2.49	10
			14	20	3.12	7
			16	20	2.38	11
			18	0	2.34	12
			19	0	2.52	12
			20	0	3.48	12
			21	0	3.21	12
			22	0	2.80	12
			23	0	2.84	12
			23	20	3.17	13
			23	40	2.37	12
		27	0	0	2.22	11
			0	40	2.08	12
			2	0	2.16	12
			3	0	1.72	10
			4	0	1.50	10
			5	0	1.32	8
			6	0	1.38	11
			7	0	1.31	10
			8	0	1.33	10
			9	0	1.17	10
			10	0	1.01	8
			11	0	0.94	9
			12	0	1.01	9
			14	0	1.22	9
			16	0	1.15	9
			18	0	1.10	8

年	月	日	時	分	H <sub>1/3</sub> (米)	T <sub>1/3</sub> (秒)
	9	17	5	0	3.13	12
			6	0	3.34	12
			7	0	3.00	11
			8	0	3.63	10
			8	40	3.62	12
			9	0	4.19	26
			9	20	3.09	11
			10	10	2.56	10
			11	0	2.64	10
			11	10	3.48	13
			11	30	3.32	11
			11	50	3.71	9
			12	0	3.38	12
			12	10	3.07	11
			12	40	3.21	10
			13	10	2.95	11
			14	0	2.97	8
			17	0	3.19	8
			19	0	3.37	10
			21	20	3.01	9
			23	0	2.83	8
	18		1	0	2.76	6
			1	30	3.97	10
			3	0	2.96	6
			5	0	2.77	7
			7	0	3.42	9
			8	40	3.14	8
			9	30	3.87	10
			9	50	3.05	12

年	月	日	時	分	$H_{\frac{1}{3}}(\text{米})$	$T_{\frac{1}{3}}(\text{秒})$
			11	30	5.29	8
			12	10	4.34	10
			12	40	4.19	11
			12	50	4.92	14
1986	9	18	13	20	4.23	7
			14	0	5.05	12
			14	10	3.95	8
			14	40	5.09	10
			15	0	4.42	6
			15	10	4.78	11
			15	20	5.08	13
			15	40	6.22	11
			16	0	7.17	15
			16	20	5.71	7
			16	50	5.11	9
			17	0	5.90	11
			17	40	6.30	8
			18	20	5.62	11
			18	50	6.36	12
			19	10	6.40	12
			19	20	8.71	8
			19	30	6.06	14
			19	40	5.77	12
			20	0	6.73	15
			20	40	4.75	10
			21	0	5.15	8
			21	50	6.29	12
			22	30	5.60	10

年	月	日	時	分	H <sub>3</sub> (米)	T <sub>3</sub> (秒)
			23	20	5.76	9
			23	50	5.64	11
1986	9	19	0	0	4.73	9
			0	10	9.93	15
			0	20	5.65	18
			0	30	9.66	9
			0	40	11.61	28
			2	0	6.83	7
			2	30	11.62	12
			2	50	9.98	9
			3	40	12.47	12
			4	0	6.85	10
			4	30	6.10	9
			5	20	6.72	10
			5	40	7.67	11
			6	10	5.48	7
			7	0	6.67	9
			7	20	9.35	15
			7	40	6.53	10
			8	10	7.05	10
			8	30	6.28	13
			8	50	7.84	12
			10	0	7.67	11
			10	20	7.27	15
			10	30	7.55	13
			10	50	6.54	8
			11	0	6.43	10
			11	10	8.43	14

年	月	日	時	分	$H_{\frac{1}{3}}$ (米)	$T_{\frac{1}{3}}$ (秒)
1986	9	19	11	40	7.27	11
			12	0	7.12	13
			12	10	6.54	10
			12	30	6.02	7
			13	0	6.25	10
			13	20	6.68	9
			14	0	6.73	11
			15	0	7.21	11
			16	0	7.30	10
			18	0	5.35	6
			20	0	4.64	8
			22	0	3.00	9
			23	0	2.55	9
		20	0	0	3.45	9
			2	0	2.73	7
			4	0	2.66	10
			6	0	2.47	9
			10	0	1.97	8